

CHAPTER 5

5.1(a) Loop

$$e = [R_1 + \frac{1}{CD}]i_1 - [\frac{1}{CD} + LD]i_2$$

$$0 = [R_2 + LD + \frac{1}{CD}]i_2 - [LD + \frac{1}{CD}]i_1$$

(b) Node

$$v_a: \quad [\frac{1}{R_1} + CD + \frac{1}{R_2}]v_a - CDv_b = \frac{1}{R_1}e$$

$$v_b: \quad [\frac{1}{LD} + CD]v_b - CDv_a = 0$$

(c) State

$$x_1 = v_c = v_a - v_b = \frac{i_c}{CD_1}$$

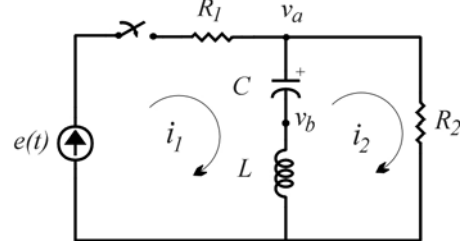
$$y_1 = v_a = v_b + v_c = \dot{x}_2 + \dot{x}_1$$

$$x_2 = i_L = \frac{v_L}{LD} = i_1 - i_2 = i_c$$

$$y_2 = v_b = v_L = L\dot{i}_L = L\dot{x}_2$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & \frac{1}{C} \\ -\frac{1}{L} & -\frac{R_1 R_2}{L(R_1 + R_2)} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{R_2}{L(R_1 + R_2)} \end{bmatrix} e$$

$$\begin{bmatrix} y_1 \\ y_2 \end{bmatrix} = \begin{bmatrix} 0 & -\frac{R_1 R_2}{(R_1 + R_2)} \\ -1 & -\frac{R_1 R_2}{(R_1 + R_2)} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} \frac{R_2}{(R_1 + R_2)} \\ \frac{R_2}{(R_1 + R_2)} \end{bmatrix} e$$



5.2(a) Loop

$$e = [R_1 + \frac{1}{CD}]i_1 - [\frac{1}{CD}]i_2$$

$$0 = [R_2 + LD + \frac{1}{CD}]i_2 - \frac{1}{CD}i_1$$

(b) Node

$$v_a: \quad [\frac{1}{R_1} + CD + \frac{1}{R_2}]v_a - \frac{1}{R_2}v_b = \frac{1}{R_1}E$$

$$v_b: \quad [\frac{1}{R_2} + \frac{1}{LD}]v_b - \frac{1}{LD}v_a = 0$$

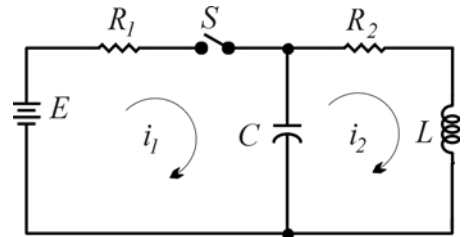
(c) State

$$x_1 = v_c = v_a$$

$$x_2 = i_L = i_2$$

$$\dot{x}_2 = \frac{v_b}{L}$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -\frac{1}{R_1 C} & -\frac{1}{C} \\ \frac{1}{L} & -\frac{R_2}{L} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} \frac{1}{R_1 C} \\ 0 \end{bmatrix} E$$

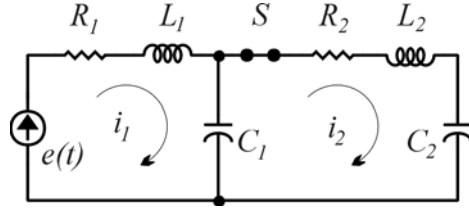


5.3 Circuit 1

(a) $e = [R_1 + L_1 D + \frac{1}{C_1 D}] i_1$ when S opens $i_2 = 0$

(b) $x_1 = v_{c_1}$ $x_2 = i_1$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & \frac{1}{C_1} \\ -\frac{1}{L_1} & -\frac{R_1}{L_1} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ \frac{1}{L_1} \end{bmatrix} e$$



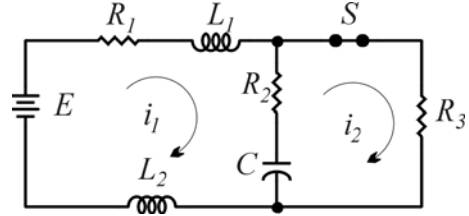
Circuit 2

(a) Similar with total resistance and inductance

$$e = [R_1 + R_2 + (L_1 + L_2)D + \frac{1}{C_1 D}] i_1$$

(b) For $x_1 = i_1$ $x_2 = v_c$

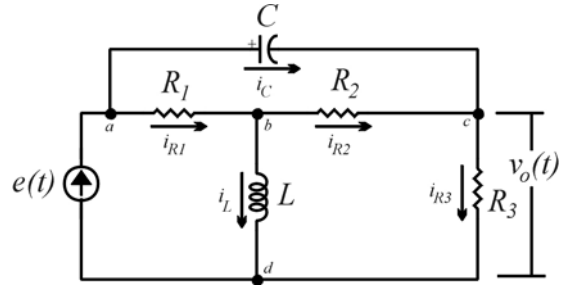
$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -\frac{R_1 + R_2}{L_1 + L_2} & -\frac{1}{L_1 + L_2} \\ \frac{1}{C} & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} \frac{1}{L_1 + L_2} \\ 0 \end{bmatrix} E$$



5.4 (a) Node d is the reference and let $v_o = v_c$.

Node b: $\left[\frac{1}{R_1} + \frac{1}{R_2} + \frac{1}{LD} \right] v_b - \frac{1}{R_1} e - \frac{1}{R_2} v_o = 0$

Node c: $-\frac{1}{R_2} v_b - CDe + \left[\frac{1}{R_2} + \frac{1}{R_3} + CD \right] v_o = 0$



(b) Use clockwise currents i_1 for abda, i_2 for bcdb & i_3 for acba.

$$[R_1 + LD] i_1 - R_1 i_2 - LD i_3 = e$$

$$-R_1 i_1 + \left[R_1 + R_2 + \frac{1}{CD} \right] i_2 - R_2 i_3 = 0$$

$$-LD i_1 - R_2 i_2 + [R_2 + R_3 + LD] i_3 = 0$$

(c) Let $x_1 = i_1, x_2 = v_c = e - v_o, u = e(t)$ then $v_b = L \dot{x}_1, y = v_o = e - x_2$

Node b: $\left[\frac{1}{R_1} + \frac{1}{R_2} \right] v_b + \frac{1}{LD} v_b - \frac{1}{R_2} v_o = \frac{1}{R_1} e$

Node c:
$$i_{R3} = i_1 + i_{R2} = x_1 + \frac{u - x_2}{R_1} - C\dot{x}_2$$

Manipulating gives:
$$\dot{x}_1 = -\frac{R_1 R_2}{L(R_1 + R_2)} x_1 - \frac{R_1}{L(R_1 + R_2)} x_2 + \frac{1}{L} u$$

$$\dot{x}_2 = \frac{R_1}{C(R_1 + R_2)} x_1 - \frac{(R_1 + R_2 + R_3)}{CR_3(R_1 + R_2)} x_2 + \frac{1}{CR_3} u$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} -\frac{R_1 R_2}{L(R_1 + R_2)} & -\frac{R_1}{L(R_1 + R_2)} \\ \frac{R_1}{C(R_1 + R_2)} & -\frac{(R_1 + R_2 + R_3)}{CR_3(R_1 + R_2)} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} \frac{1}{L} \\ \frac{1}{CR_3} \end{bmatrix} u \quad y = \begin{bmatrix} 0 & -1 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 1 \end{bmatrix} u$$

5.5 Let $x = v_c = v_o, u = e(t)$ then $i_{R1} = i_{R2} + i_c = i_{R2} + C\dot{v}_o = \frac{v_o}{R_2} + C\dot{v}_o = \frac{x}{R_2} + C\dot{x}$

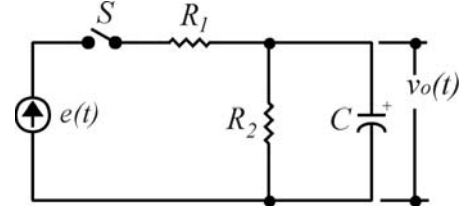
$$[R_1 + R_2]i_{R1} - R_2 i_c = e$$

$$-R_2 i_{R1} + \left[R_2 + \frac{1}{CD} \right] i_c = 0$$

$$R_1 i_{R1} + \left[\frac{1}{CD} \right] i_c = \frac{R_1 v_o}{R_2} + R_1 C\dot{v}_o + v_o = \frac{R_1 x}{R_2} + R_1 C\dot{x} + x = e$$

$$\dot{x} = -\frac{(R_1 + R_2)}{R_1 R_2 C} x + \frac{1}{R_1 C} e$$

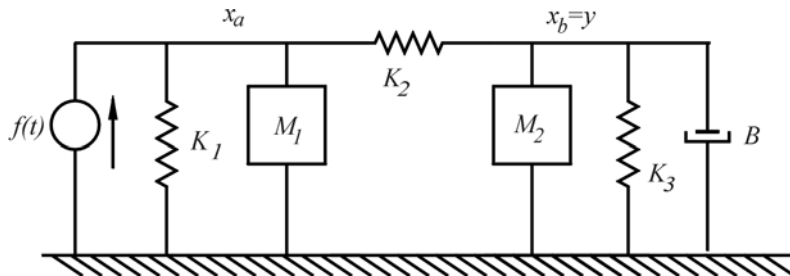
$$y = x$$



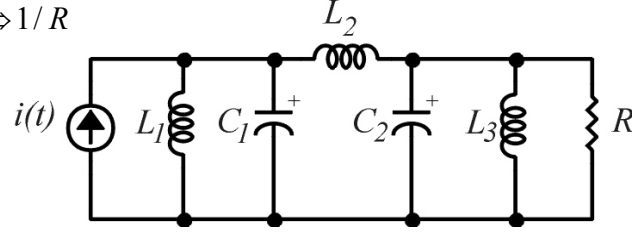
5.6 (a) $M_1 D^2 x_a = f(t) - K_1 x_a - K_2 (x_a - x_b) \Rightarrow f(t) = (M_1 D^2 + K_1 + K_2) x_a - K_2 x_b$

$$M_2 D^2 x_b = K_2 (x_a - x_b) - B D x_b - K_3 x_b \Rightarrow 0 = (M_2 D^2 + B D + K_2 + K_3) x_b - K_2 x_a$$

(b)



5.6 (c) For $f(t) \Rightarrow i(t), M \Rightarrow C, B \Rightarrow 1/L, K \Rightarrow 1/R$



(d)
$$x_a = \frac{(M_2 D^2 + BD + K_2 + K_3)}{K_2} x_b$$

$$f(t) = (M_1 D^2 + K_1 + K_2) \frac{(M_2 D^2 + BD + K_2 + K_3)}{K_2} x_b - K_2 x_b$$

$$K_2 f(t) = \{M_1 M_2 D^4 + M_1 B D^3 + [M_1 (K_2 + K_3) + M_2 (K_1 + K_2)] D^2 + (K_1 + K_2) B D + (K_1 + K_2)(K_2 + K_3)\} y - K_2^2 y$$

Given $M_1 = M_2 = I$ and $K_1 = K_2 = K_3 = K$,

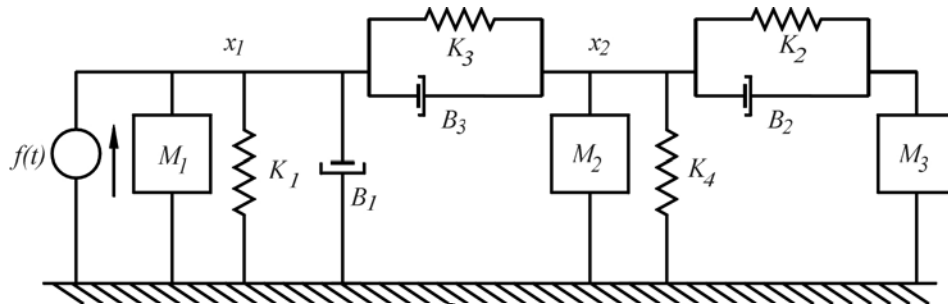
$$K f(t) = \{D^4 + B D^3 + 4 K D^2 + 2 K B D + 3 K^2\} y$$

$$G(D) = \frac{y}{f(t)} = \frac{K}{D^4 + B D^3 + 4 K D^2 + 2 K B D + 3 K^2}$$

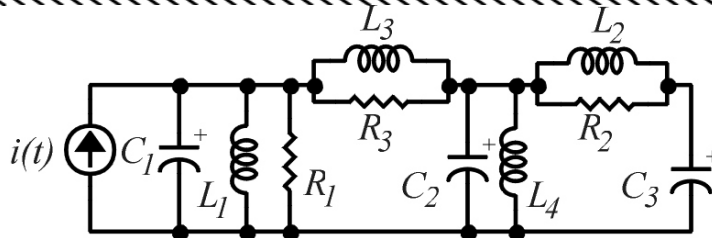
(e) Let $x_1 = x_a, x_2 = \dot{x}_1, x_3 = x_b, x_4 = \dot{x}_3, u = f(t), y = x_b = x_3$

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -2K & 0 & K & 0 \\ 0 & 0 & 0 & 1 \\ K & 0 & -2K & -B \end{bmatrix} \quad b = \begin{bmatrix} 0 \\ 1 \\ 0 \\ 0 \end{bmatrix} \quad c = [0 \quad 0 \quad 1 \quad 0]$$

5.7 (a)



(b)



5.7 (c)

$$\begin{aligned}
M_1 D^2 x_1 &= f(t) - B_1 D x_1 - K_1 x_1 - B_3 D(x_1 - x_2) - K_3(x_1 - x_2) \\
\Rightarrow f(t) &= (M_1 D^2 + B_1 D + B_3 D + K_1 + K_3)x_1 - (B_3 D + K_3)x_2 \\
M_2 D^2 x_2 &= B_3 D(x_1 - x_2) + K_3(x_1 - x_2) - K_4 x_2 - B_2 D(x_2 - x_3) - K_2(x_2 - x_3) \\
\Rightarrow 0 &= (M_2 D^2 + B_3 D + B_2 D + K_3 + K_4 + K_2)x_2 - (B_3 D + K_3)x_1 - (B_2 D + K_2)x_3 \\
M_3 D^2 x_3 &= B_2 D(x_2 - x_3) + K_2(x_2 - x_3) \\
\Rightarrow 0 &= (M_3 D^2 + B_2 D + K_2)x_3 - (B_2 D + K_2)x_2
\end{aligned}$$

(d) Let $x_1 = x_1, x_4 = \dot{x}_1, x_2 = x_2, x_5 = \dot{x}_2, x_3 = x_3, x_6 = \dot{x}_3, u = f(t)$

$$A = \begin{bmatrix} 0 & 0 & 0 & 1 & 0 & 0 \\ 0 & 0 & 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 0 & 0 & 1 \\ -\frac{(K_1 + K_3)}{M_1} & \frac{K_3}{M_1} & 0 & -\frac{(B_1 + B_3)}{M_1} & \frac{B_3}{M_1} & 0 \\ \frac{K_3}{M_2} & -\frac{(K_2 + K_3 + K_4)}{M_2} & \frac{K_2}{M_2} & \frac{B_3}{M_2} & -\frac{(B_2 + B_3)}{M_2} & \frac{B_2}{M_2} \\ 0 & \frac{K_2}{M_3} & -\frac{K_2}{M_3} & 0 & \frac{B_2}{M_3} & -\frac{B_2}{M_3} \end{bmatrix}$$

$$b^T = \begin{bmatrix} 0 & 0 & 0 & \frac{1}{M_1} & 0 & 0 \end{bmatrix}$$

5.8 (a) $3\ell f(t) = 3\ell M_2 D^2 x_c + 2\ell K_2 x_b + 2\ell B D x_b + \ell M_1 D^2 x_a + \ell K_1(x_a - x_d)$

Since $x_b = 2x_a, x_c = 3x_a$

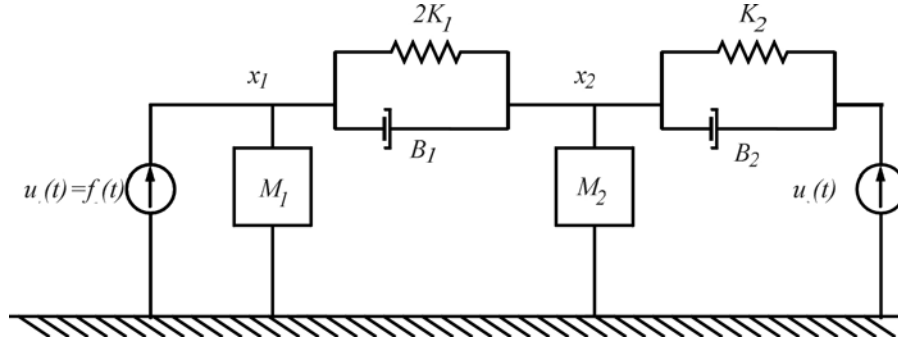
$$3\ell f(t) = 9\ell M_2 D^2 x_a + 4\ell K_2 x_a + 4\ell B D x_a + \ell M_1 D^2 x_a + \ell K_1(x_a - x_d)$$

$$M_3 D^2 x_d = K_1(x_a - x_d)$$

(b) Let $x_1 = x_a, x_2 = \dot{x}_1, x_3 = x_d, x_4 = \dot{x}_3, u = f(t)$

$$A = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -\frac{K_1 + 4K_2}{M_1 + 9M_2} & -\frac{4B}{M_1 + 9M_2} & \frac{K_1}{M_1 + 9M_2} & 0 \\ 0 & 0 & 0 & 1 \\ \frac{K_1}{M_3} & 0 & -\frac{K_1}{M_3} & 0 \end{bmatrix} \quad b = \begin{bmatrix} 0 \\ 3 \\ \frac{0}{M_1 + 9M_2} \\ 0 \\ 0 \end{bmatrix}$$

5.9 (a)



(b)
$$(M_1 D^2 + B_1 D + 2K_1)x_1 - (B_1 D + 2K_1)x_2 = u_1$$

$$-(B_1 D + 2K_1)x_1 + (M_2 D^2 + B_1 D + 2K_1 + K_2)x_2 = (B_2 D + K_2)u_2$$

(c) Let $\hat{u}_2 = (B_2 D + K_2)u_2$ be the force exerted on the tires by the road. The outputs are $y_1 = x_1$ and $y_2 = x_2$.

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -\frac{2K_1}{M_1} & \frac{2K_1}{M_1} & -\frac{B_1}{M_1} & \frac{B_1}{M_1} \\ \frac{2K_1}{M_2} & -\frac{2K_1 + K_2}{M_2} & \frac{B_1}{M_2} & -\frac{B_1 + B_2}{M_2} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 & 0 \\ 0 & 0 \\ \frac{1}{M_1} & 0 \\ 0 & \frac{1}{M_2} \end{bmatrix} \begin{bmatrix} u_1 \\ \hat{u}_2 \end{bmatrix} \quad \mathbf{y} = \begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \end{bmatrix} \mathbf{x}$$

(d) Solving the equation from part (b) with $u_1 = 0$, yields:

$$\frac{x_1}{\hat{u}_2} = \frac{(B_1 D + 2K_1)(B_2 D + K_2)}{[M_1 M_2 D^4 + (M_1 B_1 + M_1 B_2 + M_2 B_2)D^3 + (2M_1 K_1 + M_1 K_2 + B_1 B_2 + 2M_2 K_1)D^2 + (B_1 K_2 + 2B_2 K_1)D + 2K_1 K_2]}$$

5.10 (a) $[R + LD]i = e, \quad K_i i = f, \quad x_b = \frac{b}{a} x_a \Rightarrow f_b = f_a \frac{a}{b}$

$$M_2 D^2 x_b = -K_2 x_b - B D x_b + f_b \Rightarrow (M_2 D^2 + B D + K_2)x_b = f_b = \frac{a}{b} f_a$$

$$M_1 D^2 x_a = -K_1 x_a - f_a + f \Rightarrow (M_1 D^2 + K_1)x_a + f_a = K_i i \Rightarrow (M_1 D^2 + K_1)x_a - K_i i = -f_a$$

$$(M_2 D^2 + B D + K_2)x_b = \frac{a}{b} f_a = -\frac{a}{b} [(M_1 D^2 + K_1)x_a - K_i i]$$

$$(M_2 D^2 + B D + K_2)x_b = -\frac{a}{b} \left[(M_1 D^2 + K_1) \frac{a}{b} x_b - K_i i \right] = \frac{a K_i}{b} i - \frac{a^2}{b^2} (M_1 D^2 + K_1)x_b$$

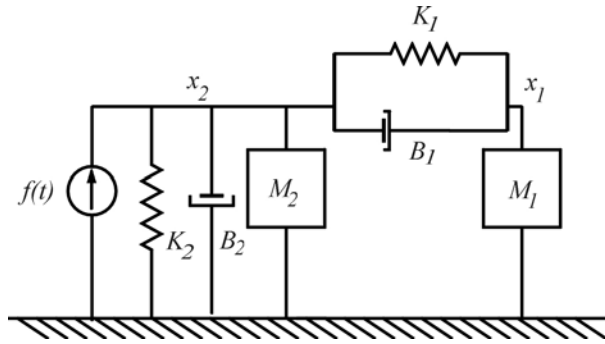
$$(M_2 + \frac{a^2}{b^2} M_1) D^2 x_b + B D x_b + (K_2 + \frac{a^2}{b^2} K_1)x_b = \frac{a K_i}{b} i$$

$$L D i = -R i + e,$$

5.10 (b) Let $x_1 = x_b, x_2 = \dot{x}_1, x_3 = i, u = e$

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 & 0 \\ -\frac{K_2 + \frac{a^2}{b^2}K_1}{M_2 + \frac{a^2}{b^2}M_1} & -\frac{B}{M_2 + \frac{a^2}{b^2}M_1} & \frac{aK_i}{b(M_2 + \frac{a^2}{b^2}M_1)} \\ 0 & 0 & -\frac{R}{L} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ \frac{1}{L} \end{bmatrix} e \quad \mathbf{y} = [1 \quad 0 \quad 0] \mathbf{x}$$

5.11 (a)



(b) $(M_1 D^2 + B_1 D + K_1)x_1 - (B_1 D + K_1)x_2 = 0$
 $-(B_1 D + K_1)x_1 + [M_2 D^2 + (B_1 + B_2)D + (K_1 + K_2)]x_2 = f$

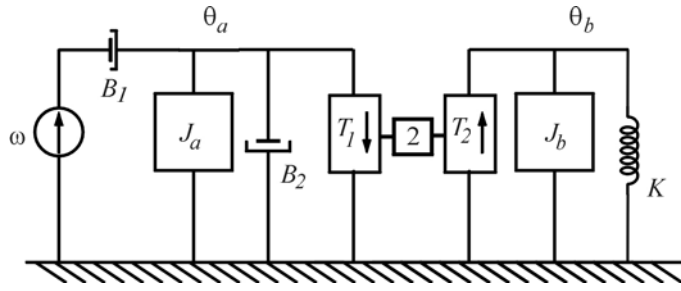
(c) Let $x_1 = x_1, x_2 = x_2, x_3 = \dot{x}_1, x_4 = \dot{x}_2, u = f(t)$

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \\ -\frac{K_1}{M_1} & \frac{K_1}{M_1} & -\frac{B_1}{M_1} & \frac{B_1}{M_1} \\ \frac{K_1}{M_2} & -\frac{K_1 + K_2}{M_2} & \frac{B_1}{M_2} & -\frac{B_1 + B_2}{M_2} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ \frac{1}{M_2} \end{bmatrix} f \quad \mathbf{y} = [1 \quad 0 \quad 0 \quad 0] \mathbf{x}$$

(d)

$$G = \frac{x_1}{f} = \frac{(B_1 D + K_1)}{[M_1 M_2 D^4 + (M_1 B_1 + M_1 B_2 + M_2 B_1)D^3 + (M_1 K_1 + M_1 K_2 + M_2 K_1 + B_1 B_2)D^2 + (B_1 K_2 + B_2 K_1)D + K_1 K_2]}$$

5.12 (a)



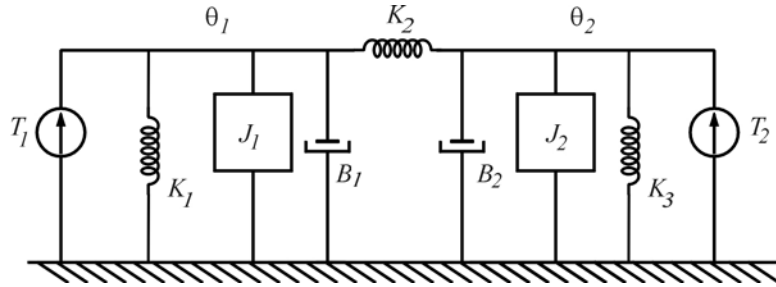
$$\begin{aligned}
 (b) \quad T_1 &= -(J_a D^2 + B_2 D) \theta_a + B_1 \omega & T_2 &= 2T_1 = (J_b D^2 + K) \theta_b \\
 2T_1 &= -2(J_a D^2 + B_2 D) \theta_a + 2B_1 \omega = (J_b D^2 + K) \theta_b \\
 -2(J_a D^2 + B_2 D) 2\theta_b + 2B_1 \omega &= (J_b D^2 + K) \theta_b \\
 (J_b + 2J_a) D^2 \theta_b &= 2J_b D^2 \theta_b = -(4B_2 D + K) \theta_b + 2B_1 \omega
 \end{aligned}$$

$$(c) \quad \dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 \\ \frac{-K}{2J_b} & \frac{-2B_2}{J_b} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ \frac{B_1}{J_b} \end{bmatrix} \omega$$

$$(d) \quad (2J_b D^2 + 4B_2 D + K) \theta_b = 2B_1 \omega$$

$$\frac{\theta_b}{\omega} = \frac{2B_1}{2J_b D^2 + 4B_2 D + K}$$

5.13 (a)



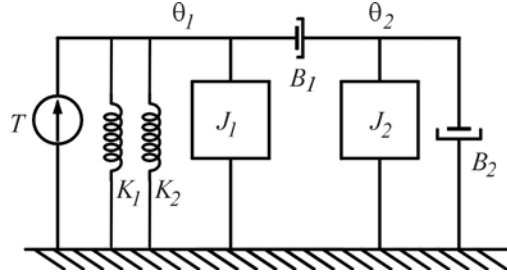
$$(b) \quad T_1 = (J_1 D^2 + B_1 D + K_1 + K_2) \theta_1 - K_2 \theta_2$$

$$T_2 = (J_2 D^2 + B_2 D + K_3 + K_2) \theta_2 - K_2 \theta_1$$

$$(c) \quad \text{Let } x_1 = \theta_1, x_2 = \dot{\theta}_1, x_3 = \theta_2, x_4 = \dot{\theta}_2$$

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -\frac{K_1 + K_2}{J_1} & -\frac{B_1}{J_1} & \frac{K_2}{J_1} & 0 \\ 0 & 0 & 1 & 0 \\ \frac{K_2}{J_2} & 0 & -\frac{K_3 + K_2}{J_2} & -\frac{B_2}{J_2} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 & 0 \\ \frac{1}{J_1} & 0 \\ 0 & 0 \\ 0 & \frac{1}{J_2} \end{bmatrix} \begin{bmatrix} T_1 \\ T_2 \end{bmatrix}$$

5.14 (a)



$$(b) \quad J_1 D^2 \theta_1 = -B_1 D(\theta_1 - \theta_2) - (K_1 + K_2) \theta_1 + T \quad J_2 D^2 \theta_2 = B_1 D(\theta_1 - \theta_2) - B_2 D \theta_2$$

$$(c) \quad \text{Let } x_1 = \theta_1, x_2 = \dot{\theta}_1, x_3 = \theta_2, x_4 = \dot{\theta}_2$$

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -\frac{K_1 + K_2}{J_1} & -\frac{B_1}{J_1} & 0 & \frac{B_1}{J_1} \\ 0 & 0 & 1 & 0 \\ 0 & \frac{B_1}{J_2} & 0 & -\frac{B_1 + B_2}{J_2} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ \frac{1}{J_1} \\ 0 \\ 0 \end{bmatrix} T$$

$$(d) \quad (J_1 D^2 + B_1 D + K_1 + K_2) \theta_1 - T = B_1 D \theta_2$$

$$[J_2 D^2 + (B_1 + B_2) D] \theta_2 = B_1 D \theta_1$$

$$\frac{[J_2 D^2 + (B_1 + B_2) D]}{B_1 D} \theta_2 = \theta_1$$

$$(J_1 D^2 + B_1 D + K_1 + K_2) \frac{[J_2 D^2 + (B_1 + B_2) D]}{B_1 D} \theta_2 - T = B_1 D \theta_2$$

$$\frac{(J_1 D^2 + B_1 D + K_1 + K_2)[J_2 D^2 + (B_1 + B_2) D] - (B_1 D)^2}{B_1 D} \theta_2 = T$$

$$\frac{\theta_2}{T} = \frac{B_1}{J_1 J_2 D^3 + (J_2 B_1 + J_1 B_1 + J_1 B_2) D^2 + (J_2 K_1 + J_2 K_2 + B_1 B_2) D + (K_1 + K_2)(B_1 + B_2)}$$

$$5.15 \quad J_1 D^2 \theta_1 = T_1 \quad T_1 = (n_a)_{2,1} T_{2o} \quad T_{2o} = T_{2i} - J_2 D^2 \theta_2 \quad T_{2i} = (n_a)_{3,2} T_{3o}$$

$$T_{3o} = T - J_3 D^2 \theta_3 \quad (n_a)_{2,1} = \theta_2 / \theta_1 \quad (n_a)_{3,2} = \theta_3 / \theta_2$$

$$J_1 D^2 \theta_1 = (n_a)_{2,1} ((n_a)_{3,2} (T - J_3 D^2 \theta_3) - J_2 D^2 \theta_2)$$

$$J_1 D^2 \theta_1 = (n_a)_{2,1} ((n_a)_{3,2} (T - (n_a)_{2,1} (n_a)_{3,2} J_3 D^2 \theta_1) - (n_a)_{2,1} J_2 D^2 \theta_1)$$

$$J_1 D^2 \theta_1 = (n_a)_{2,1} ((n_a)_{3,2} (T - (n_a)_{2,1} (n_a)_{3,2} J_3 D^2 \theta_1) - (n_a)_{2,1} J_2 D^2 \theta_1)$$

$$\left[J_1 + (n_a)_{2,1}^2 (n_a)_{3,2} J_2 + (n_a)_{2,1}^2 (n_a)_{3,2}^2 J_3 \right] D^2 \theta_1 = (n_a)_{2,1} (n_a)_{3,2} T$$

$$\left[\frac{1}{(n_a)_{2,1} (n_a)_{3,2}} J_1 + (n_a)_{2,1} J_2 + (n_a)_{2,1} (n_a)_{3,2} J_3 \right] D^2 \theta_1 = T = J_{eq} \dot{\omega} \quad \dot{\omega} = \frac{T}{J_{eq}}$$

System 1

(a)

$$J_{eq} = \frac{1}{48} J_1 + 4J_2 + 48J_3$$

$$J_{eq} = 52.02J_3$$

System 2

$$J_{eq} = \frac{1}{48} J_1 + 8J_2 + 48J_3$$

$$J_{eq} = 56.02J_3$$

System 1 accelerates faster due to a lower equivalent inertia.

(b)

$$J_{eq} = \frac{1}{48} J_1 + 4J_2 + 48J_3$$

$$J_{eq} = \left(\frac{100}{48} + 160 + 48 \right) J_3 = 210.08J_3$$

$$J_{eq} = \frac{1}{48} J_1 + 8J_2 + 48J_3$$

$$J_{eq} = \left(\frac{100}{48} + 320 + 48 \right) J_3 = 370.08J_3$$

Again, System 1 accelerates faster due to a lower equivalent inertia.

5.16 (a) $T = (JD^2 + B_1D)\theta + rf \quad (MD^2 + B_2D + K)x = f \quad \theta r = x$

$$T = \frac{(JD^2 + B_1D)}{r}x + r(MD^2 + B_2D + K)x$$

(b)

$$T = \frac{(J + Mr^2)D^2 + (B_1 + B_2r^2)D + Kr^2}{r}x \Rightarrow \frac{x}{T} = \frac{r}{(J + Mr^2)D^2 + (B_1 + B_2r^2)D + Kr^2}$$

(c) Let $x_1 = x, x_2 = \dot{x}_1, u = T$

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 \\ -\frac{Kr^2}{J + Mr^2} & -\frac{B_1 + B_2r^2}{J + Mr^2} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ \frac{r}{J + Mr^2} \end{bmatrix} T$$

5.17 (a) Let $x_1 = \theta_3, x_2 = \dot{\theta}_3, x_3 = \dot{\theta}_2, y = \theta_3, u = T$

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 & 0 \\ -\frac{K_2}{J_2} & -\frac{B_2 + B_3}{J_2} & \frac{B_3}{J_2} \\ 0 & \frac{B_3}{J_1} & -\frac{B_1 + B_3}{J_1} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ \frac{1}{J_1} \end{bmatrix} T \quad \mathbf{y} = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \mathbf{x}$$

(b) Let $x_1 = \theta_3, x_2 = \dot{\theta}_3, x_3 = \theta_2, x_4 = \dot{\theta}_2, y = \theta_3, u = \theta_1$

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 & 0 & 0 \\ -\frac{K_2}{J_2} & -\frac{B_2 + B_3}{J_2} & 0 & \frac{B_3}{J_2} \\ 0 & 0 & 1 & 0 \\ 0 & \frac{B_3}{J_1} & -\frac{K_1}{J_1} & -\frac{B_1 + B_3}{J_1} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ 0 \\ \frac{K_1}{J_1} \end{bmatrix} \theta_1 \quad \mathbf{y} = \begin{bmatrix} 1 & 0 & 0 & 0 \end{bmatrix} \mathbf{x}$$

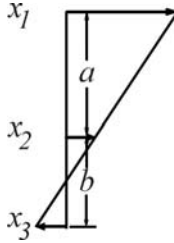
$$5.18 \quad x_2 = x'_2 - x''_2 = \frac{b}{a+b} x_1 - \frac{a}{a+b} x_3 \quad (1) \quad x'_2 \text{ is due to motion, } x'_2 \text{ and } x''_2 \text{ are due to } x_3$$

$$Dy_1 = C_1 x_2 \quad (2)$$

$$x_3 = y_2 = \frac{d}{c+d} y_1 \quad (3)$$

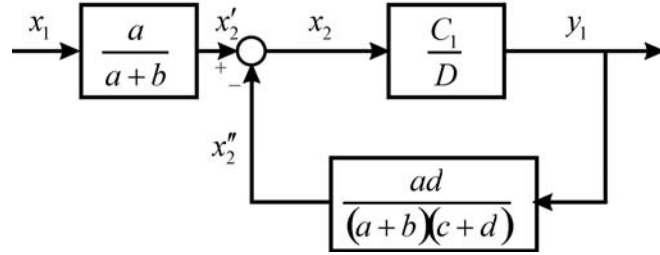
$$\left[\frac{C_1 a d}{(a+b)(c+d)} + D \right] y_1 \approx \frac{C_1 b}{a+b} x_1 \quad (4)$$

From similar triangles:



$$\frac{x_1 - x_2}{a} = \frac{x_1 + x_3}{a+b} \quad (5)$$

The block diagram representation is:



- (b) If the load has mass and damping, the equation for piston motion is derived in Sec. 5.9. Starting with Eq. (5.107) but using the symbols of this problem gives

$$\left[\frac{VM}{K_B C} \right] D^3 y_1 + \left[\frac{VB}{K_B C} + \frac{M}{C} (L + C_p) \right] D^2 y_1 + \left[C_b + \frac{B}{C} (L + C_p) \right] D y_1 = C_x x_2 \quad (6)$$

Combining Eq. (6) and Eq (1) and (3) gives:

$$\left[\frac{VM}{K_B C} \right] D^3 y_1 + \left[\frac{VB}{K_B C} + \frac{M}{C} (L + C_p) \right] D^2 y_1 + \left[C_b + \frac{B}{C} (L + C_p) \right] D y_1 + \left[\frac{C_x a d}{(a+b)(c+d)} \right] y_1 = \frac{C_x b}{a+b} x_1$$

5.19

$$\dot{\mathbf{x}} = \begin{bmatrix} 0 & 1 & 0 \\ -\frac{K}{M} & -\frac{B}{M} & \frac{C}{M} \\ 0 & -\frac{C_b K_B}{V} & -\frac{K_B(L + C_p)}{V} \end{bmatrix} \mathbf{x} + \begin{bmatrix} 0 \\ 0 \\ \frac{K_B C_x}{V} \end{bmatrix} u \quad \mathbf{y} = \begin{bmatrix} 1 & 0 & 0 \end{bmatrix} \mathbf{x}$$

5.20 Rewrite Eq. (5.116) in terms of pressure (or head), i.e., $P(\text{or } h)=qR$. Thus the pressure drop in the pipes are $P_1=q_1R_1$, $P_2=q_2R_2$, and $P_3=q_3R_3$. Since

$$q_3 = q_1 + q_2 \quad (1) \quad P_3 = q_3R_3 = \left[\frac{P_1}{R_1} + \frac{P_2}{R_2} \right] R_3 \quad (2)$$

The pressure at the junction of pipes 1 and 2 is P_3 . This pressure is equal to the liquid level in tanks 1 and 2 minus the pressure drop in pipes 1 and 2, respectively. Thus

$$h_1 - P_1 = P_3 \quad (3) \quad h_2 - P_2 = P_3 \quad (4)$$

Solving for P_1 and P_2 in terms of h_1 and h_2 yields:

$$P_1 = \frac{R_1(R_2 + R_3)}{R} h_1 - \frac{R_1R_3}{R} h_2 \quad (5) \quad P_2 = -\frac{R_2R_3}{R} h_1 + \frac{R_2(R_1 + R_3)}{R} h_2 \quad (6)$$

Where $R = R_1R_2 + R_2R_3 + R_1R_3$

Using Eq. (5.116), the change in head in tank 1 when q_A is larger than q_1 is

$$Dh_1 = q_A - q_1 = q_A - \frac{P_1}{R_1} \quad (8) \quad \text{for tank 2:} \quad Dh_2 = q_B - q_2 = q_B - \frac{P_2}{R_2} \quad (9)$$

Using Eqs. (5) and (6) in Eqs. (8) and (9) yields the state equations

$$\dot{h}_1 = -\left[\frac{R_2 + R_3}{R} \right] h_1 + \frac{R_3}{R} h_2 + q_A \quad (10) \quad \dot{h}_2 = \frac{R_3}{R} h_1 - \left[\frac{R_1 + R_3}{R} \right] h_2 + q_B \quad (11)$$

$$5.21 \quad e = R_a i_a + L_a D i_a + e_b = R_a i_a + L_a D i_a + K_b D \theta_m \quad (1)$$

$$T = K_T i_a = J D^2 \theta_m + B D \theta_m \quad (2) \quad i_a = \frac{J}{K_T} D^2 \theta_m + \frac{B}{K_T} D \theta_m \quad (3)$$

$$e = \frac{L_a J}{K_T} D^3 \theta_m + \frac{R_a J + L_a B}{K_T} D^2 \theta_m + \frac{R_a B + K_b K_T}{K_T} D \theta_m \quad (4)$$

5.22 (a) The basic equation of the system is of the form $T = J\ddot{\theta}$. All of the torques in the system are summed about the pivot point P. The force f exerts a torque $f\ell \cos \theta$ about P, the force Mg exerts a torque $-Mg\ell \sin \theta$ about P, and the damper exerts the torque $-B\dot{\theta}$ about P. Therefore the equation of motion is

$$J D^2 \theta = M\ell^2 D^2 \theta = f\ell \cos \theta - Mg\ell \sin \theta - B D \theta \quad (1)$$

(b) For small angles θ , Eq. (1) becomes

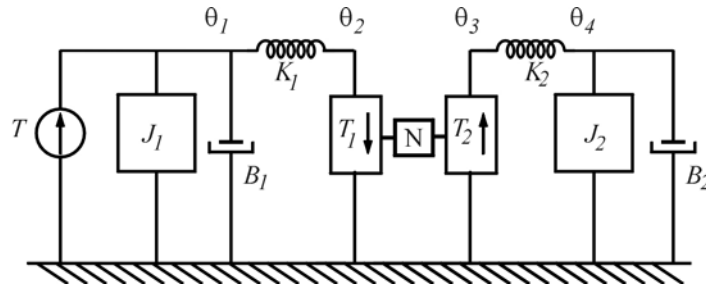
$$M\ell^2 D^2 \theta = f\ell - Mg\ell \theta - B D \theta \quad (2)$$

(c)

$$\ddot{\theta} = \frac{f}{M\ell} - \frac{g}{\ell} \theta - \frac{B}{M\ell^2} \dot{\theta} \quad (3)$$

$$\begin{bmatrix} \dot{x}_1 \\ \dot{x}_2 \end{bmatrix} = \begin{bmatrix} 0 & 1 \\ -\frac{g}{\ell} & -\frac{B}{M\ell^2} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} + \begin{bmatrix} 0 \\ 1 \\ M\ell^2 \end{bmatrix} f \quad y = \begin{bmatrix} 1 & 0 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} \quad (4)$$

5.23 (a)



$$(b) \quad J_1 D^2 \theta_1 = -B_1 D \theta_1 - K_1 (\theta_1 - \theta_2) + T \quad J_2 D^2 \theta_4 = K_2 (\theta_3 - \theta_4) - B_2 D \theta_4$$

$$T_1 = K_1 (\theta_1 - \theta_2) \quad T_2 = N T_1 (\theta_2 = N \theta_3) \quad T_2 = K_2 (\theta_3 - \theta_4)$$

5.24 (a) From Prob 5.21, Eq. (2) is modified to

$$T = K_T i_a = JD^2 \theta_m + BD \theta_m + K \theta_m \quad i_a = \frac{J}{K_T} D^2 \theta_m + \frac{B}{K_T} D \theta_m + \frac{K}{K_T} \theta_m$$

Solving for i_a and substituting into Eq. (1) yields:

$$e = R_a \left(\frac{J}{K_T} D^2 \theta_m + \frac{B}{K_T} D \theta_m + \frac{K}{K_T} \theta_m \right) + L_a D \left(\frac{J}{K_T} D^2 \theta_m + \frac{B}{K_T} D \theta_m + \frac{K}{K_T} \theta_m \right) + K_b D \theta_m$$

$$e = \frac{L_a J}{K_T} D^3 \theta_m + \left(\frac{R_a J + L_a B}{K_T} \right) D^2 \theta_m + \left(\frac{R_a B + L_a K}{K_T} + K_b \right) D \theta_m + \frac{R_a K}{K_T} \theta_m$$

$$K_T v_1 = L_a J D^3 \theta_m + (R_a J + L_a B) D^2 \theta_m + (R_a B + L_a K + K_b K_T) D \theta_m + R_a K \theta_m$$

(b) Since $\omega_m(t) = D \theta_m(t)$

$$\frac{\theta_m(t)}{v_1(t)} = \frac{K_T}{L_a J D^3 + (R_a J + L_a B) D^2 + (R_a B + L_a K + K_b K_T) D + R_a K}$$

$$\frac{\omega_m(t)}{v_1(t)} = \frac{K_T D}{L_a J D^3 + (R_a J + L_a B) D^2 + (R_a B + L_a K + K_b K_T) D + R_a K}$$