

## Chapter 2

2.1. A plane wave has an electric field given by  $\vec{E} = E_0 \sin(kz - \omega t + \phi) \hat{x}$  is incident on a material with a susceptibility given by  $\chi = (1 + \sqrt{3}i)\chi_0 / 2$ .

a) What is the complex amplitude of the electric field?

$$\underline{A} = E_0 e^{i(\phi - \frac{\pi}{2})} \hat{x} \quad (S2.1)$$

b) What is the phase shift between a polarization induced by the field and the incident field?

The relationship between the polarization's complex amplitude and the field's complex amplitude is,

$$\underline{P} = \epsilon_0 \chi \underline{A} \quad (S2.2)$$

Therefore the phase difference is the phase of the complex susceptibility, which is  $\frac{\pi}{3}$ .

c) What is the real polarization in this medium induced by the field?

$$\vec{P} = \epsilon_0 \chi_0 E_0 \sin\left(kz - \omega t + \phi + \frac{\pi}{3}\right) \hat{x} \quad (S2.3)$$

or equivalently,

$$\vec{P} = \epsilon_0 \chi_0 E_0 \cos\left(kz - \omega t + \phi - \frac{\pi}{6}\right) \hat{x} \quad (S2.4)$$

2.2. A plane wave in a vacuum has an electric field given by,  $\vec{E} = E_0 \cos(kz - \omega t + \phi) \hat{x}$ .

a) What is  $\vec{B}$ ?

We use Maxwell's equation, 2.2, to relate the curl of the electric field to the time derivative of the magnetic field. For a field of the form given here,  $\nabla \rightarrow ik\hat{z}$  and  $\frac{\partial}{\partial t} \rightarrow -i\omega$ . Therefore,

$$\vec{B} = \frac{E_0}{c} \cos(kz - \omega t + \phi) \hat{y} \quad (S2.5)$$

b) What is the complex amplitude of  $\vec{B}$ ?

$$\underline{B} = \frac{E_0}{c} e^{i\phi} \hat{y} \quad (S2.6)$$

c) What are  $\vec{S}$  and  $\langle \vec{S} \rangle$ ?

$$\vec{S} = \vec{E} \times \vec{H} = \frac{\vec{E} \times \vec{B}}{\mu_0} = \frac{E_0^2}{\mu_0 c} \cos^2(kz - \omega t + \phi) \hat{z} \quad (S2.7)$$

$$\langle \vec{S} \rangle = \frac{E_0^2}{2\mu_0 c} \hat{z} \quad (S2.8)$$

2.3. Consider two monochromatic quantities,  $\vec{F} = \frac{1}{2} \vec{F} e^{i\omega t} + \text{c.c.}$  and  $\vec{G} = \frac{1}{2} \vec{G} e^{i\omega t} + \text{c.c.}$ . Prove that

$$\langle \vec{F} \cdot \vec{G} \rangle = \frac{1}{2} \text{Re}(\vec{F} \cdot \vec{G}^*), \text{ where } \langle \rangle \text{ denotes a time average.}$$

$$\vec{F} \cdot \vec{G} = \frac{1}{4} (\vec{F} \cdot \vec{G} e^{i2\omega t} + \vec{F} \cdot \vec{G}^* + \text{c.c.}) \quad (\text{S2.9})$$

Note that any complex number,  $z$ , plus its complex conjugate,  $z^*$ , is  $z+z^*=2\text{Re}(z)$ . Therefore,

$$\vec{F} \cdot \vec{G} = \frac{1}{2} (\text{Re}(\vec{F} \cdot \vec{G} e^{i2\omega t}) + \text{Re}(\vec{F} \cdot \vec{G}^*)). \quad (\text{S2.10})$$

The first term on the right hand side is proportional to  $\cos(2\omega t)$  and it therefore time-averages to zero. Hence,

$$\langle \vec{F} \cdot \vec{G} \rangle = \frac{1}{2} \text{Re}(\vec{F} \cdot \vec{G}^*). \quad (\text{S2.11})$$

- 2.4. Use Poynting's theorem and Equation 2.39 to determine the phase difference between an incident monochromatic plane-wave field and the induced polarization that leads to (a) maximum attenuation, and (b) maximum gain of the incident beam. Use this result to comment on whether the polarization should lead or lag with respect to the incident field for 1) attenuation and 2) gain.

Taking the time-average of Poynting's theorem gives

$$\left\langle \int_{\text{closed surface}} \vec{S} \cdot d\vec{a} \right\rangle = - \left\langle \int \vec{E} \cdot \frac{\partial \vec{P}}{\partial t} dV \right\rangle \quad (\text{S2.12})$$

The left-hand side is the time-averaged power flow out of a closed surface. Hence, when

$$\left\langle \vec{E} \cdot \frac{d\vec{P}}{dt} \right\rangle < 0 \quad (\text{S2.13})$$

more power flows out of the surface than flows in (gain). When this expression is greater than zero net power flows into the surface (attenuation). For monochromatic plane waves,

$$\left\langle \vec{E} \cdot \frac{d\vec{P}}{dt} \right\rangle = \frac{1}{2} \text{Re} \left( \vec{A} \cdot \left( \frac{d\vec{P}}{dt} \right)^* \right) = \frac{1}{2} \text{Re} (i\omega \vec{A} \cdot \vec{P}^*) \quad (\text{S2.14})$$

(see Problem 2.3) where  $\vec{A}$  and  $\vec{P}$  are complex amplitudes. Let's simplify the expression by substituting

$\vec{A} = \vec{E}_0 e^{i\phi_E}$  and  $\vec{P} = \vec{P}_0 e^{i\phi_P}$  so that

$$\frac{1}{2} \text{Re} (i\omega \vec{A} \cdot \vec{P}^*) = \frac{\omega}{2} \vec{A}_0 \cdot \vec{P}_0 \text{Re} (ie^{i(\phi_E - \phi_P)}) = \frac{\omega}{2} \vec{A}_0 \cdot \vec{P}_0 \sin(\phi_P - \phi_E) \quad (\text{S2.15})$$

Maximum gain and attenuation occur when  $P$  and  $A$  are  $90^\circ$  out of phase. a) Maximum gain

occurs when  $(\phi_P - \phi_E) = -\frac{\pi}{2}$  and b) maximum attenuation occurs when  $(\phi_P - \phi_E) = \frac{\pi}{2}$ .

Equation (S2.15) also shows that when the polarization phase is greater than the field (ie leads in phase) then attenuation occurs, and gain occurs when the polarization lags with respect to the field.

- 2.5. Show that absorption is linear in the sense that when two inputs at different frequencies are present in a medium that

$$\left\langle \vec{E}_{\text{total}} \cdot \frac{d\vec{P}_{\text{total}}}{dt} \right\rangle = \left\langle \vec{E}_1 \cdot \frac{d\vec{P}_1}{dt} \right\rangle + \left\langle \vec{E}_2 \cdot \frac{d\vec{P}_2}{dt} \right\rangle. \quad 2.140$$

Use monochromatic plane waves for  $\vec{E}_1(\omega_1)$  and  $\vec{E}_2(\omega_2)$ . The polarization's complex amplitude is related to the field via  $\vec{P} = \epsilon_0 \chi \vec{A}$ . Assume that the susceptibility is the same for both frequencies.

The total field is given by,

$$\vec{E}_{\text{Tot}} = \frac{1}{2} \left[ \vec{A}_1 e^{-i\omega_1 t} + \vec{A}_2 e^{-i\omega_2 t} + \text{c.c.} \right]. \quad (\text{S2.16})$$

The time derivative of the total polarization is, given our assumptions,

$$\frac{d\vec{P}_{\text{Tot}}}{dt} = \frac{1}{2} \left[ -i\varepsilon_0 \chi \omega_1 \vec{A}_1 e^{-i\omega_1 t} - i\varepsilon_0 \chi \omega_2 \vec{A}_2 e^{-i\omega_2 t} + \text{c.c.} \right]. \quad (\text{S2.17})$$

We take the dot-product of Equations (S2.16) and (S2.17),

$$\vec{E}_{\text{Tot}} \cdot \frac{d\vec{P}_{\text{Tot}}}{dt} = \frac{1}{4} \left[ \vec{A}_1 e^{-i\omega_1 t} + \vec{A}_2 e^{-i\omega_2 t} + \text{c.c.} \right] \cdot \left[ -i\varepsilon_0 \chi \omega_1 \vec{A}_1 e^{-i\omega_1 t} - i\varepsilon_0 \chi \omega_2 \vec{A}_2 e^{-i\omega_2 t} + \text{c.c.} \right]. \quad (\text{S2.18})$$

Taking the time average of Equation (S2.18) leaves us with

$$\left\langle \vec{E}_{\text{Tot}} \cdot \frac{d\vec{P}_{\text{Tot}}}{dt} \right\rangle = \frac{1}{4} i\varepsilon_0 (\chi^* - \chi) \left[ \omega_1 |\vec{A}_1|^2 + \omega_2 |\vec{A}_2|^2 \right] = \frac{1}{2} \varepsilon_0 \text{Im}(\chi) \left[ \omega_1 |\vec{A}_1|^2 + \omega_2 |\vec{A}_2|^2 \right]. \quad (\text{S2.19})$$

To evaluate the right-hand side of 2.140, we use Equation (S2.11) for each term, for example,

$$\left\langle \vec{E}_1 \cdot \frac{d\vec{P}_1}{dt} \right\rangle = \frac{1}{2} \text{Re} \left( i\varepsilon_0 \omega_1 \chi^* |\vec{A}_1|^2 \right) = \frac{1}{2} \varepsilon_0 \omega_1 \text{Im}(\chi) |\vec{A}_1|^2. \quad (\text{S2.20})$$

Hence

$$\left\langle \vec{E}_1 \cdot \frac{d\vec{P}_1}{dt} \right\rangle + \left\langle \vec{E}_2 \cdot \frac{d\vec{P}_2}{dt} \right\rangle = \frac{1}{2} \varepsilon_0 \text{Im}(\chi) \left[ \omega_1 |\vec{A}_1|^2 + \omega_2 |\vec{A}_2|^2 \right], \quad (\text{S2.21})$$

and this equation is equal to the left hand side of Equation 2.140 as shown in (S2.19).

2.6. Show that, when the electric field is of the form  $\text{Re} \{ E_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)} \hat{E} \}$

$$\nabla \cdot \vec{E} = \text{Re} \left( i\vec{k} \cdot \vec{E}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)} \right)$$

$$\nabla \times \vec{E} = \text{Re} \left( i\vec{k} \times \vec{E}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)} \right)$$

$$\nabla^2 \vec{E} = \text{Re} \left( -|\vec{k}|^2 \vec{E}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)} \right)$$

That is, for monochromatic plane waves  $\nabla \rightarrow i\vec{k}$  and  $\frac{\partial}{\partial t} \rightarrow -i\omega$ .

These relations may be directly written out. Another approach is to consider that any combination of  $\vec{\nabla}$  operations results in a function of  $\frac{\partial}{\partial x}$ ,  $\frac{\partial}{\partial y}$ , and  $\frac{\partial}{\partial z}$ , which we will call

$f\left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z}\right)$ . To see the result of this function operating on a monochromatic field of the

form,  $E_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)} \hat{E}$ , we note that the only spatial dependence comes in the  $\vec{k} \cdot \vec{r}$  term. Hence,

$f\left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z}\right)$  operating on  $E_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)} \hat{E}$  is written as

$$(E_0 \hat{E}) f\left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z}\right) \exp\{i(k_x x + k_y y + k_z z - \omega t)\}. \quad (\text{S2.22})$$

The action of  $\frac{\partial}{\partial x}$ ,  $\frac{\partial}{\partial y}$ , and  $\frac{\partial}{\partial z}$  on the exponential term is illustrated by considering

$$\frac{\partial}{\partial x} \left[ \exp i(k_x x + k_y y + k_z z - \omega t) \right] = i k_x \left[ \exp i(k_x x + k_y y + k_z z - \omega t) \right].$$

Hence  $\frac{\partial}{\partial x}$ ,  $\frac{\partial}{\partial y}$ , and  $\frac{\partial}{\partial z}$  operating on  $e^{i(\vec{k} \cdot \vec{r} - \omega t)}$  give back  $e^{i(\vec{k} \cdot \vec{r} - \omega t)}$  multiplied by  $ik_x$ ,  $ik_y$ , and  $ik_z$

respectively. Since the operations return the  $e^{i(\vec{k} \cdot \vec{r} - \omega t)}$  multiplied by a constant, successive operations of partial derivatives result in  $e^{i(\vec{k} \cdot \vec{r} - \omega t)}$  multiplied by the appropriate constants.

Therefore  $f\left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z}\right)e^{i(\vec{k} \cdot \vec{r} - \omega t)} = f(ik_x, ik_y, ik_z)e^{i(\vec{k} \cdot \vec{r} - \omega t)}$ . Similarly,

$$f\left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z}\right)\text{Re}\left(\bar{E}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}\right) = \text{Re}\left(f\left(\frac{\partial}{\partial x}, \frac{\partial}{\partial y}, \frac{\partial}{\partial z}\right)\bar{E}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}\right) = \text{Re}\left(f(ik_x, ik_y, ik_z)\bar{E}_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}\right). \quad (\text{S2.23})$$

Hence, we may identify,

$$\nabla = \frac{\partial}{\partial x} \hat{x} + \frac{\partial}{\partial y} \hat{y} + \frac{\partial}{\partial z} \hat{z} \rightarrow ik_x \hat{x} + ik_y \hat{y} + ik_z \hat{z} = i\vec{k} \quad (\text{S2.24})$$

A similar argument yields,  $\frac{\partial}{\partial t} \rightarrow -i\omega$ .

2.7. Use the Kronecker-delta properties to prove that  $\chi_{\alpha\beta} = R_{i\alpha} R_{j\beta} \chi'_{ij}$  can be “inverted” to give  $\chi'_{ij} = R_{i\alpha} R_{j\beta} \chi_{\alpha\beta}$ .

Operate on both sides,

$$R_{i\alpha} \chi_{\alpha\beta} = R_{i\alpha} R_{j\beta} \chi'_{ij} = \delta_{\alpha\alpha'} R_{j\beta} \chi'_{ij} \quad (\text{S2.25})$$

The Kronecker-delta gives  $\alpha=\alpha'$ ,

$$R_{i\alpha} \chi_{\alpha\beta} = R_{j\beta} \chi'_{ij} \quad (\text{S2.26})$$

Similarly, we operate on both sides again,

$$R_{j\beta} R_{i\alpha} \chi_{\alpha\beta} = R_{j\beta} R_{j\beta'} \chi'_{ij} = \delta_{\beta\beta'} \chi'_{ij} \quad (\text{S2.27})$$

The Kronecker-delta gives  $\beta=\beta'$ , and we have the final result,

$$R_{j\beta} R_{i\alpha} \chi_{\alpha\beta} = \chi'_{ij}. \quad (\text{S2.28})$$

2.8. Use the constitutive relationship, Equation 2.5, along with Equation 2.45 to prove that  $\epsilon_{ij} = \epsilon_o (\delta_{ij} + \chi_{ij})$ .

Substituting Equation 2.45 into Equation 2.5 (written in component form) gives

$$D_i = \epsilon_o A_i + \epsilon_o \chi_{ij} A_j \quad (\text{S2.29})$$

This is equivalent to

$$D_i = \epsilon_o \delta_{ij} A_j + \epsilon_o \chi_{ij} A_j = \epsilon_o (\delta_{ij} + \chi_{ij}) A_j. \quad (\text{S2.30})$$

Furthermore,  $D_i = \epsilon_{ij} A_j$  so that we may equate

$$\epsilon_{ij} = \epsilon_o (\delta_{ij} + \chi_{ij}) \quad (\text{S2.31})$$

2.9. In Chapter 3, we show that the second order nonlinear polarization is given in component form as

$$P_i^{(2)} = \epsilon_o \chi_{ijk}^{(2)} A_j A_k, \quad 2.145$$

where  $\chi_{ijk}^{(2)}$  is the second order susceptibility and  $A_j$  is a component of the incident field's complex amplitude.

Use Equation 2.145 to prove that  $\chi_{ijk}^{(2)}$  is a rank 3 tensor.

We prove that  $\chi_{ijk}^{(2)}$  is a rank 3 tensor by showing that it transforms like a tensor. We start by noting that the polarization and field are vectors and hence we can rewrite them according to tensor transformations. Specifically, we may write them with respect to a different coordinate system. For the purposes of this example,  $ijk$  refer to one coordinate system and  $\alpha\beta\gamma$  to the other. A given polarization transforms like,

$$\mathbf{P}_i^{(2)} = \mathbf{R}_{i\alpha} \mathbf{P}_\alpha^{(2)}. \quad (\text{S2.32})$$

We transform the polarization and fields in Equation 2.145,

$$\mathbf{R}_{i\alpha} \mathbf{P}_\alpha^{(2)} = \epsilon_0 \chi_{ijk}^{(2)} (\mathbf{R}_{j\beta} \mathbf{A}_\beta) (\mathbf{R}_{k\gamma} \mathbf{A}_\gamma) = \epsilon_0 \mathbf{R}_{j\beta} \mathbf{R}_{k\gamma} \chi_{ijk}^{(2)} \mathbf{A}_\beta \mathbf{A}_\gamma \quad (\text{S2.33})$$

Next operate on both sides,

$$\mathbf{R}_{i'\alpha'} \mathbf{R}_{i\alpha} \mathbf{P}_\alpha^{(2)} = \delta_{i'i} \mathbf{P}_{\alpha'}^{(2)} = \epsilon_0 \mathbf{R}_{i'\alpha'} \mathbf{R}_{j\beta} \mathbf{R}_{k\gamma} \chi_{ijk}^{(2)} \mathbf{A}_\beta \mathbf{A}_\gamma \quad (\text{S2.34})$$

Hence,

$$\mathbf{P}_{\alpha'}^{(2)} = \epsilon_0 (\mathbf{R}_{i\alpha} \mathbf{R}_{j\beta} \mathbf{R}_{k\gamma} \chi_{ijk}^{(2)}) \mathbf{A}_\beta \mathbf{A}_\gamma \quad (\text{S2.35})$$

In the transformed coordinate system we identify,

$$\mathbf{R}_{i\alpha} \mathbf{R}_{j\beta} \mathbf{R}_{k\gamma} \chi_{ijk}^{(2)} = \chi_{\alpha\beta\gamma}^{(2)} \quad (\text{S2.36})$$

Next we “invert” the relationship by operating on both sides (see also Problem 2.7),

$$\mathbf{R}_{i\alpha'} \mathbf{R}_{i\alpha} \mathbf{R}_{j\beta} \mathbf{R}_{k\gamma} \chi_{ijk}^{(2)} = \mathbf{R}_{i\alpha'} \chi_{\alpha\beta\gamma}^{(2)} \quad (\text{S2.37})$$

Note that  $\mathbf{R}_{i\alpha'} \mathbf{R}_{i\alpha} = \delta_{\alpha'\alpha}$ , so that  $\mathbf{R}_{j\beta} \mathbf{R}_{k\gamma} \chi_{ijk}^{(2)} = \mathbf{R}_{i\alpha} \chi_{\alpha\beta\gamma}^{(2)}$ . Similarly, we operate on both sides of this equation with  $\mathbf{R}_{j\beta'}$  and  $\mathbf{R}_{k\gamma'}$  yielding

$$\chi_{ijk}^{(2)} = \mathbf{R}_{i\alpha} \mathbf{R}_{j\beta} \mathbf{R}_{k\gamma} \chi_{\alpha\beta\gamma}^{(2)}. \quad (\text{S2.38})$$

Therefore the second order susceptibility transforms as a rank 3 tensor.

2.10. Find the principal indices of refraction (eigenvalues) and the direction of the principal axes (eigenvectors) for the following relative dielectric tensor,  $\tilde{\epsilon}_r$ ,

$$\begin{bmatrix} 2.5 & .5 & 0 \\ .5 & 2.5 & 0 \\ 0 & 0 & 4 \end{bmatrix}. \quad 2.146$$

The eigenvalues are found from

$$\begin{vmatrix} 2.5 - \lambda & .5 & 0 \\ .5 & 2.5 - \lambda & 0 \\ 0 & 0 & 4 - \lambda \end{vmatrix} = 0 \quad (\text{S2.39})$$

Solving for  $\lambda$  gives  $\lambda_1=2$ ,  $\lambda_2=3$ , and  $\lambda_3=4$ .

The corresponding indices are  $n_1=\sqrt{2}$ ,  $n_2=\sqrt{3}$ , and  $n_3=2$ . The eigenvector corresponding to

$$\lambda_1 \text{ is } \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ -1 \\ 0 \end{pmatrix}, \quad (\text{S2.40})$$

$$\text{for } \lambda_2 \text{ is } \frac{1}{\sqrt{2}} \begin{pmatrix} 1 \\ 1 \\ 0 \end{pmatrix}, \quad (\text{S2.41})$$

$$\text{and for } \lambda_3 \text{ is } \begin{pmatrix} 0 \\ 0 \\ 1 \end{pmatrix}. \quad (\text{S2.42})$$

2.11. An electric field in a material that has a dielectric tensor as given in Problem 2.10 has a complex amplitude,

$$\tilde{\mathbf{E}} = (\hat{x} + \hat{y} + \hat{z}) \frac{E_0}{\sqrt{3}}. \quad \text{What is the complex amplitude of the displacement vector, } \tilde{\mathbf{D}}? \text{ Show that } \tilde{\mathbf{D}} \text{ and } \tilde{\mathbf{E}}$$

are not parallel, and find the angle between them.

We use  $\mathbf{D}_i = \epsilon_0 \epsilon_{ij} \mathbf{E}_j$ , which in matrix form is,

$$\vec{D} = \epsilon_0 \begin{bmatrix} 2.5 & .5 & 0 \\ .5 & 2.5 & 0 \\ 0 & 0 & 4 \end{bmatrix} \begin{bmatrix} 1 \\ 1 \\ 1 \end{bmatrix} \frac{E_0}{\sqrt{3}} = \epsilon_0 \frac{(3\hat{x} + 3\hat{y} + 4\hat{z})}{\sqrt{3}} E_0 \quad (\text{S2.43})$$

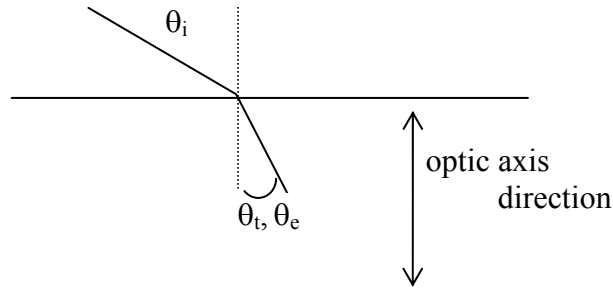
Clearly  $\vec{D}$  and  $\vec{E}$  are not parallel. We find the angle between the two vectors by taking the dot-product of their unit-vectors:

$$\cos \rho = \hat{\vec{D}} \cdot \hat{\vec{E}} = \frac{(3\hat{x} + 3\hat{y} + 4\hat{z}) \cdot (\hat{x} + \hat{y} + \hat{z})}{\sqrt{34} \cdot \sqrt{3}} = \frac{10}{\sqrt{102}} = 0.99$$

The angle is 0.14 rads or  $8.0^\circ$ .

- 2.12. A uniaxial crystal of indices  $n_o$  and  $n_z$  is cut so that the optic axis is perpendicular to the surface. Show that for a beam incident on the interface from air at an angle of incidence,  $\theta_i$ , that the angle of refraction of the e-wave is

$$\tan \theta_e = \frac{n_z}{n_o} \frac{\sin \theta_i}{\sqrt{n_z^2 - \sin^2 \theta_i}}. \quad 2.147$$



Since the optic axis and the surface normal are parallel,  $\theta_e = \theta_t$ . Snell's law is  $n_i \sin \theta_i = n_t \sin \theta_t (= n_e \sin \theta_e)$

where  $n_i=1$  and we substitute in for the extraordinary index,

$$\sin \theta_i = \left( \frac{\cos^2 \theta_e}{n_o^2} + \frac{\sin^2 \theta_e}{n_z^2} \right)^{-1/2} \sin \theta_e \quad (\text{S2.44})$$

Rearranging gives,

$$\left( \frac{1}{\tan^2 \theta_e n_o^2} + \frac{1}{n_z^2} \right) = \frac{1}{\sin^2 \theta_i} \quad (\text{S2.45})$$

Solving for  $\tan \theta_e$ ,

$$\tan \theta_e = \frac{n_z}{n_o} \frac{\sin \theta_i}{\sqrt{n_z^2 - \sin^2 \theta_i}} \quad (\text{S2.46})$$

- 2.13. The law of reflection in crystals is not always intuitively obvious. In a derivation similar to that for Snell's law, reflections satisfy the equation  $n_i \sin \theta_i = n_r \sin \theta_r$ , where  $\theta_i$  and  $\theta_r$  are the incident angle and reflected angle with respect to the surface normal respectively;  $n_i$  and  $n_r$  are the indices for the incident and reflected beams. As the following example shows, in crystals it is possible that  $n_i \neq n_r$  and therefore  $\theta_r \neq \theta_i$ . A right prism, shown in Figure 2.13, is made out of a uniaxial birefringent crystal with the optic axis as shown in the figure. The principal indices are  $n_o=2.2$  and  $n_z=2.1$  and the prism angles are  $45^\circ$  and  $90^\circ$ . The incident beam of light is linearly polarized in the vertical direction (parallel to the optic axis). Calculate the reflected angle with respect to the reflected surface normal (dotted line). Note that it is not  $45^\circ$ !

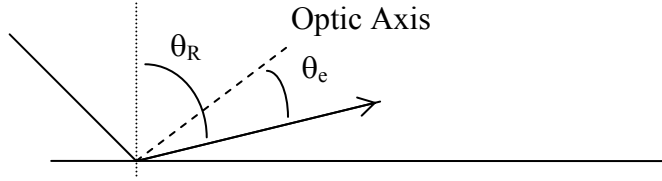


Figure S2.1. Geometry for Problem 2.13.

Figure S2.1 shows the geometry with respect to the reflecting interface. The incident angle is  $45^\circ$ . Let's assume that the reflected angle is slightly larger than  $45^\circ$  as shown in Figure S2.1. We have

$$n_i \sin \theta_i = n_R \sin \theta_R = n_R (\theta_e) \sin \left( \theta_e + \frac{\pi}{4} \right). \quad (\text{S2.47})$$

The incident beam is polarized along the crystal's z-axis so  $n_i = n_z$ . The incident angle is  $\theta_i = \pi/4$ , and we use a standard trig identity to expand,

$$\sin \left( \theta_e + \frac{\pi}{4} \right) = \frac{\sin \theta_e + \cos \theta_e}{\sqrt{2}} \quad (\text{S2.48})$$

Making the above substitutions along with the extraordinary index of the reflected wave in Equation (S2.47) gives

$$n_z = \left( \frac{\cos^2 \theta_e}{n_o^2} + \frac{\sin^2 \theta_e}{n_z^2} \right)^{-1/2} (\sin \theta_e + \cos \theta_e) \quad (\text{S2.49})$$

After some algebraic manipulation we obtain,

$$\tan \theta_e = \frac{n_z^2 - n_o^2}{2n_o^2} \quad (\text{S2.50})$$

Substituting in  $n_o = 2.2$  and  $n_z = 2.1$  gives  $\theta_e = -44 \text{ mrad} (= -2.5^\circ)$ . So the reflected angle is  $\theta_R = 42.5^\circ$ .

- 2.14. A linear-optical effect that plays a role in ultrashort-pulse nonlinear optics is the group velocity mismatch between different carrier frequencies. For example, in second harmonic generation the fundamental and second harmonic will temporally separate due to group velocity mismatch. The group velocity is given by

$$v_g = \frac{\partial \omega}{\partial k}, \text{ however, it is easier to calculate inverse group velocity } v_g^{-1} = \frac{\partial k}{\partial \omega}. \text{ Plot the group velocity as a}$$

function of wavelength for an o-wave traveling through BBO (see Appendix B for Sellmeier Equations. Based on the group velocity evaluated at  $0.532$  and  $1.064 \mu\text{m}$ , over what propagation distance in the BBO will a  $100 \text{ fs}$  pulse at  $0.532$  temporally separate from a  $100 \text{ fs}$   $1.064 \mu\text{m}$  pulse? Define temporal separation when the pulses are separated by  $100 \text{ fs}$ .

The inverse group velocity is given by

$$v_g^{-1} = \frac{\partial k}{\partial \omega} = \frac{n}{c} \left( 1 - \frac{\lambda}{n} \frac{dn}{d\lambda} \right) \quad (\text{S2.51})$$

Using the Sellmeier Equations in Appendix B allows us to obtain  $n(\lambda)$  and  $dn/d\lambda$ . A plot of the group velocity is given in Figure S2.2. A direct calculation at  $1.064$  and  $0.532 \mu\text{m}$  gives for the group velocity,

$$v_g(1.064 \mu\text{m}) = 1.972 \times 10^8 \text{ m/s}$$

$$v_g(0.532 \mu\text{m}) = 1.742 \times 10^8 \text{ m/s}$$

A  $100 \text{ fsec}$  pulse corresponds to approximately  $30 \mu\text{m}$  spatial extent (in vacuum). Therefore the pulses are separated when their peaks are spaced roughly  $30 \mu\text{m}$  apart. The separation between the two pulses is

$$\Delta x = |v_1 - v_2| t \quad (\text{S2.52})$$

where  $v_1$  and  $v_2$  are the group velocities and  $t=0$  corresponds to when the two pulses are coincident in time. Using  $\Delta x=30\mu\text{m}$  and using the group velocities given above, we obtain  $t=6.05 \times 10^{-12}\text{s}$  as the period of time it takes the two pulses to separate. In this time the  $1.064\mu\text{m}$  pulse travels 1.08 mm and the  $0.532\mu\text{m}$  pulse travels 1.05 mm. Therefore after 1 mm the two pulses separate. Note that a longer interaction length is possible by timing the pulses so that the  $0.532\mu\text{m}$  pulse arrives first (it travels slower). In this way, a 2 mm interaction length is possible.

c) From the plot,  $\lambda_F=2.03\mu\text{m}$  and  $\lambda_{\text{SHG}}=1.015$  have the same group velocity.

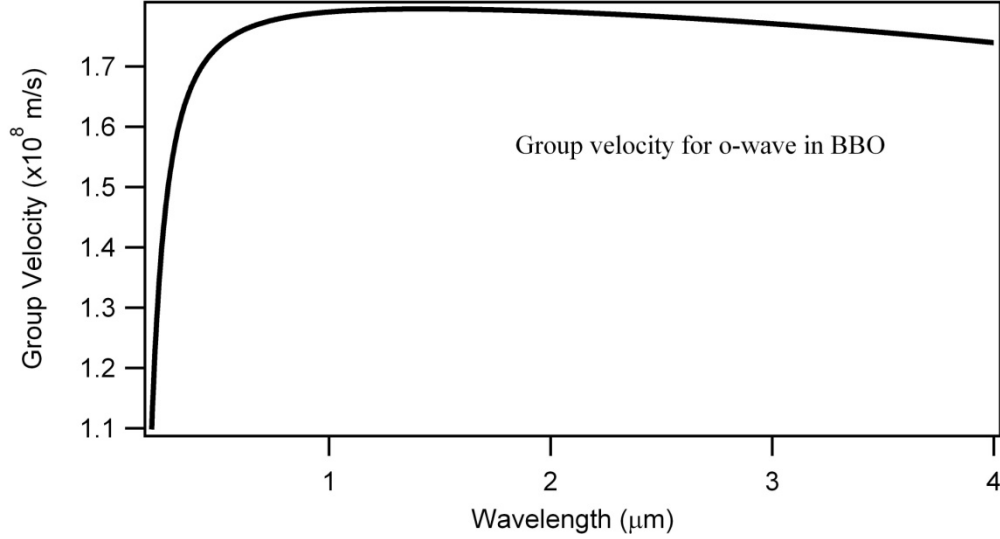


Figure S2.2. Group velocity in BBO.

2.15. Derive the wave equation in an isotropic medium for the case where  $j_f$  is not equal to zero. Assume monochromatic plane waves and use Ohm's law to relate the complex amplitudes of the free current density and the field, ie.  $\vec{j}_f = \sigma \vec{A}$ .

a) Show that the resultant index of refraction is complex.

b) Show that the imaginary part of the index leads to attenuation as the field propagates through the medium.

a) The wave equation is

$$\nabla \times (\nabla \times \vec{E}) = -\mu_0 \frac{\partial}{\partial t} \nabla \times \vec{H}. \quad (\text{S2.53})$$

Similar to the derivation for the lossless case, this equation becomes

$$-\nabla^2 \vec{E} = -\mu_0 \frac{\partial}{\partial t} \left( \vec{j}_f + \frac{\partial \vec{D}}{\partial t} \right). \quad (\text{S2.54})$$

The complex amplitude of  $\vec{D}$  is related to that of the field,  $\vec{E}$  via  $\vec{D} = \epsilon_0 \epsilon_r \vec{A}$ . For

monochromatic plane waves of the form  $\vec{A} e^{i(\vec{k} \cdot \vec{r} - \omega t)}$  we replace  $\vec{\nabla} \rightarrow i\vec{k}$  and  $\frac{\partial}{\partial t} \rightarrow -i\omega$ . After

making these substitutions we arrive at,

$$|\vec{k}|^2 = \left( i\omega\mu_0\sigma_0 + \frac{\epsilon_r\omega^2}{c^2} \right) = \frac{\epsilon_r\omega^2}{c^2} \left( 1 + i \frac{\sigma_0}{\epsilon_0\epsilon_r\omega} \right). \quad (\text{S2.55})$$



We see that the plane wave solution requires a complex k-vector. From the relationship,

$\tilde{k} = \frac{\tilde{n}\omega}{c}$ , we obtain the complex index,

$$\tilde{n} = \frac{\sqrt{\epsilon_r}\omega}{c} \left( 1 + i \frac{\sigma_0}{\epsilon_0 \epsilon_r \omega} \right)^{1/2}. \quad (\text{S2.56})$$

b) Rewriting  $\tilde{n} = n + i\kappa$  gives  $\tilde{k} = (n + i\kappa) \frac{\omega}{c}$ . Therefore the plane wave solution is of the form

$$\bar{A} \exp i \left( (n + i\kappa) \frac{\omega}{c} z - \omega t \right) = \bar{A} \exp(-\kappa z) \exp i \left( \frac{n\omega}{c} z - \omega t \right) \quad (\text{S2.57})$$

where we have chosen the direction of propagation to be the z-direction. This solution shows that the field exponentially decays with a decay constant given by the imaginary part of the index.

- 2.16. A new transparent material has been discovered and before nonlinear optics experiments can be performed, we need to know it's dispersion curve. Measurements of the index of refraction are made at five wavelengths (using five different lasers). Table 2.1 below gives the results of the measurements.

Table 2.1 Index as a function of wavelength

Wavelength ( $\mu\text{m}$ )	Index of refraction
0.330	2.47379
0.532	2.23421
0.6328	2.20271
1.064	2.15601
1.57	2.1375
2.804	2.1029

Fit the above data using a two-pole Sellmeier equation,

$$n^2(\lambda) = A_0 + \frac{\lambda^2 A_1}{\lambda^2 - A_2} + \frac{\lambda^2 A_3}{\lambda^2 - A_4}$$

where  $\lambda$  is kept in units of microns. The stability of the fitting routine requires reasonable guesses for the fitting parameters.  $A_2$  and  $A_4$  correspond to the IR and UV poles, so set the starting guesses accordingly. If we assume that the dispersion is relatively "slow" then the index should not be a strong function of wavelength. From the data we see that it has a value centered on approximately 2.2. Hence a good guess for  $A_0$  is  $\sim 2.2^2$ . After performing the fitting routine, give the values for the fit parameters  $A_0$  through  $A_4$ . Plot the measured and fitted index of refraction as a function of wavelength on the same graph. Check to be sure that  $A_2$  and  $A_4$  give poles in the IR and UV respectively.

The fit and fitting parameters are shown in Figure S2.3. From the fit values we see a UV pole at  $0.211 \mu\text{m}$  and an IR pole at  $114 \mu\text{m}$ .

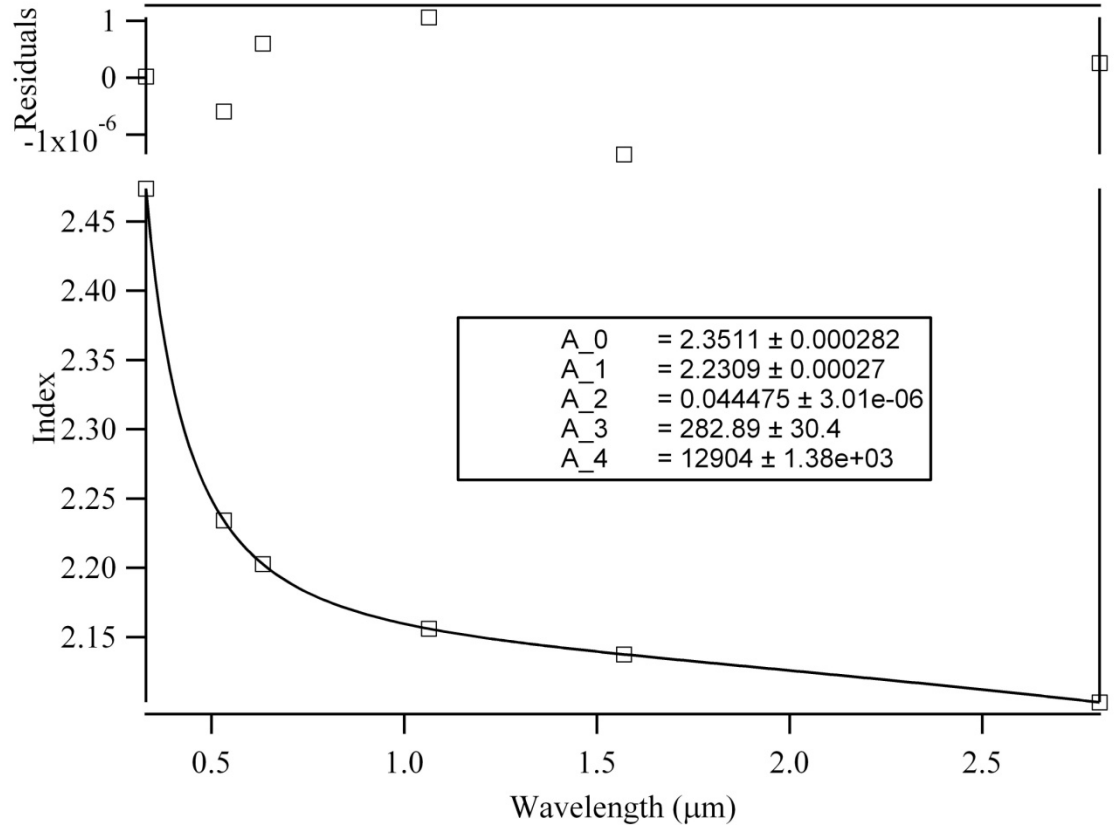


Figure S2.3. Data and fit solution for Problem 2.16.

- 2.17. Use Equation 2.100 to show that the two eigen-polarizations are orthogonal. Hint, show that the D-vectors corresponding to the two eigen-indices are orthogonal.

Fresnel's equation states:

$$\frac{s_x^2}{\frac{1}{n_x^2} - \frac{1}{n^2}} + \frac{s_y^2}{\frac{1}{n_y^2} - \frac{1}{n^2}} + \frac{s_z^2}{\frac{1}{n_z^2} - \frac{1}{n^2}} = 0, \text{ or } \sum_i \frac{s_i^2}{\frac{1}{n_i^2} - \frac{1}{n^2}} = 0 \quad (\text{S2.58})$$

This equation has two solutions, which we call  $n_1$  and  $n_2$ . The D-vectors associated with these values of  $n$  are perpendicular by showing that their dot-product is zero.

Equation 2.100 is,

$$D_i = \frac{(\hat{\mathbf{k}} \cdot \vec{\mathbf{E}}) s_i}{\mu c^2 \left[ \frac{1}{n_i^2} - \frac{1}{n^2} \right]} \quad (\text{S2.59})$$

And hence

$$\vec{D}_{n1} \cdot \vec{D}_{n2} = \sum_i \frac{1}{\mu c^2} \frac{(\hat{\mathbf{k}} \cdot \vec{\mathbf{E}}) s_i^2}{\left( \frac{1}{n_1^2} - \frac{1}{n^2} \right) \left( \frac{1}{n_2^2} - \frac{1}{n^2} \right)} \quad (\text{S2.60})$$

Using the method of partial fractions,

$$\vec{D}_{n1} \cdot \vec{D}_{n2} = \frac{(\hat{k} \cdot \vec{E})}{\mu c^2} \frac{n_1^2 n_2^2}{n_2^2 - n_1^2} \sum_i s_i^2 \left[ \frac{1}{\left( \frac{1}{n_i^2} - \frac{1}{n_1^2} \right)} - \frac{1}{\left( \frac{1}{n_i^2} - \frac{1}{n_2^2} \right)} \right] = \frac{(\hat{k} \cdot \vec{E})}{\mu c^2} \frac{n_1^2 n_2^2}{n_2^2 - n_1^2} \left[ \sum_i \frac{s_i^2}{\left( \frac{1}{n_i^2} - \frac{1}{n_1^2} \right)} - \sum_i \frac{s_i^2}{\left( \frac{1}{n_i^2} - \frac{1}{n_2^2} \right)} \right]$$

Notice that both sums in the square brackets are solutions to Fresnel's equation ( $n_1$  and  $n_2$ ) and hence are both equal to zero. Therefore  $\vec{D}_{n1} \cdot \vec{D}_{n2} = 0$  proving that  $\vec{D}_{n1}$  is perpendicular to  $\vec{D}_{n2}$ .

- 2.18. Calculate the angle where  $n_e = n_o$  in the  $xz$  plane of a biaxial crystal. This angle is the angle of the optic axis with respect to the  $z$ -axis. Use the Sellmeier equations for KTP to plot the angle of the optic axis with respect to the  $z$ -axis as a function of wavelength from 0.5 to 4.0  $\mu m$ .

The intersection is given by

$$\frac{\cos^2 \theta}{n_x^2} + \frac{\sin^2 \theta}{n_z^2} = \frac{1}{n_y^2} \quad (S2.61)$$

Solving for angle gives,

$$\sin^2 \theta = \frac{n_z^2}{n_y^2} \left( \frac{n_x^2 - n_y^2}{n_x^2 - n_z^2} \right) \quad (S2.62)$$

The dispersion of the optic-axis angle is shown in Figure S2.4.

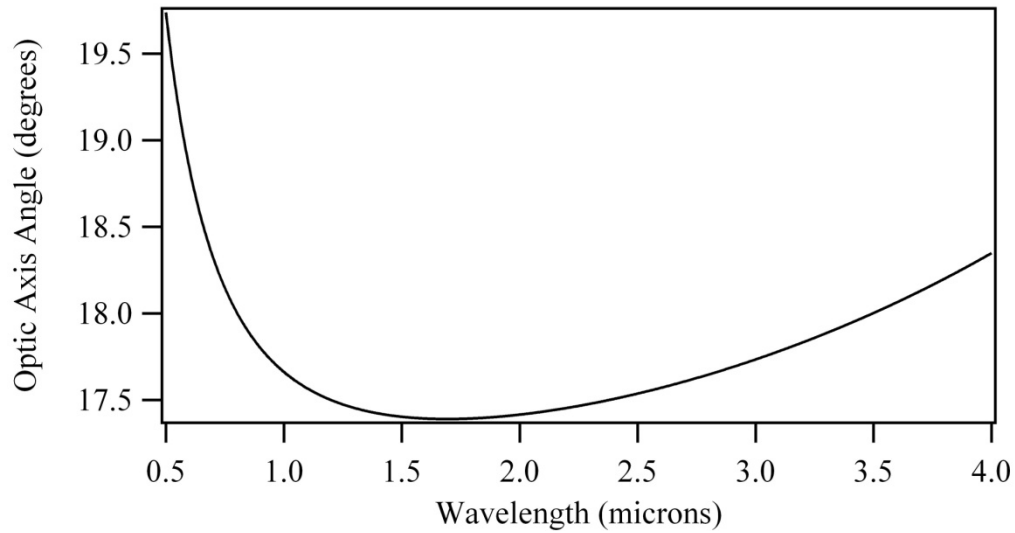


Figure S2.4. Dispersion of the optic axis angle.

- 2.19. Give expressions for  $n_e$  in each of the principal planes of a biaxial crystal. In the  $xz$ - and  $yz$ - planes, assume that the  $k$ -vector propagates at an angle,  $\theta$ , with respect to the  $z$ -axis. In the  $xy$ -plane, assume that the  $k$ -vector propagates at an angle,  $\phi$ , with respect to the  $x$ -axis.

$xy$ -plane:

$$n_e(\phi) = \left[ \frac{\cos^2 \phi}{n_y^2} + \frac{\sin^2 \phi}{n_x^2} \right]^{-1/2} \quad (S2.63)$$

$xz$ -plane:

$$n_e(\theta) = \left[ \frac{\cos^2 \theta}{n_x^2} + \frac{\sin^2 \theta}{n_z^2} \right]^{-1/2} \quad (S2.64)$$

yz-plane:

$$n_e(\theta) = \left[ \frac{\cos^2 \theta}{n_y^2} + \frac{\sin^2 \theta}{n_z^2} \right]^{-1/2} \quad (\text{S2.65})$$

- 2.20. Nonlinear optical interactions typically involve multiple beams at multiple wavelengths. If the beams have different polarizations, then they may walk off each other as the following example demonstrates. Two beams of light, one at 600 nm (o-polarized) and the other at 300 nm (e-polarized), are sent through a BBO crystal with their k-vectors at an angle of 40.5 degrees to the optic axis. The BBO crystal is 2 cm long. The beam diameters are the same and are given by "D". Determine the distance in the crystal where the two beams walk off each other. Define beam separation when the centers of the beams are displaced by one beam diameter. For what beam diameters is the full crystal length used? Sellmeier equations for BBO are found in Appendix B.

The beams walk off each other (using the definitions of walked-off as given in the problem statement) at a distance,

$$L = \frac{D}{\tan \rho} \quad (\text{S2.66})$$

where  $\rho$  is the walk-off angle of the e-wave. The walk-off angle is given by Equation 2.106,

$$\rho = \tan^{-1} \left( \frac{n_o^2}{n_z^2} \tan \theta \right) - \theta. \quad (\text{S2.67})$$

The walk-off angle is evaluated for the e-wave at 300 nm (the o-wave at 600 nm has no walk-off). The walk-off angle is, 82mrad (4.73°). So the effective crystal length is 12D.

- 2.21. In the following, use the Sellmeier Equations for BBO found in Appendix B.

- a) Make a plot  $n_e(\theta)$  from  $\theta=0$  to  $\pi/2$  for both  $\lambda=1.064 \mu\text{m}$  and  $\lambda=0.532 \mu\text{m}$ . Include on the same graph  $n_o(\lambda)$  for both wavelengths.

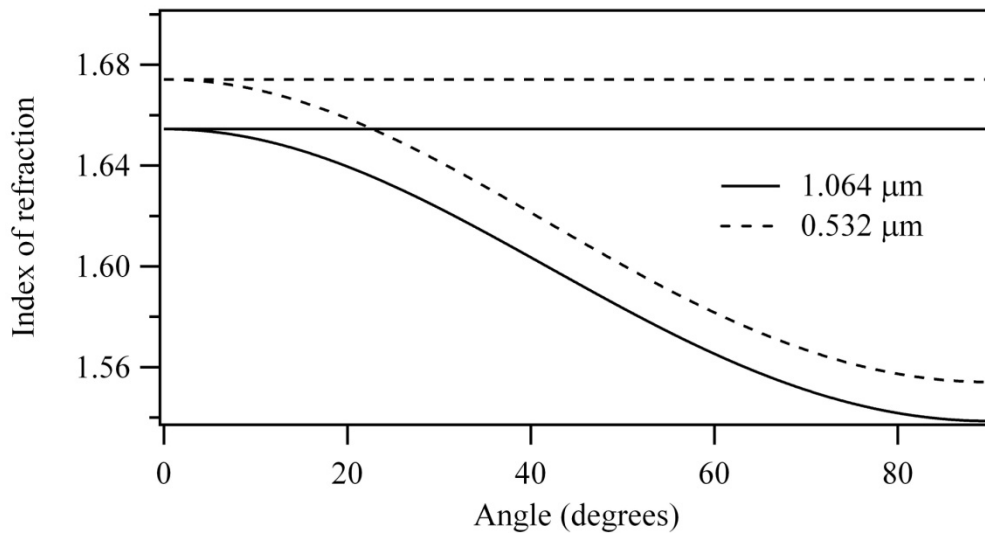


Figure S2.5. Plot of  $n_e$  and  $n_o$  for 1.064 and 0.532  $\mu\text{m}$ . The horizontal lines correspond to the ordinary index.

- b) Is BBO positive or negative uniaxial?

Negative uniaxial

- c) For what polarization states and for what angle does  $n(1.064) = n(0.532)$ ? Hint, this corresponds to the intersection of two of the curves in part (a). This angle is the phase matching angle for second harmonic generation.

When the  $0.532 \mu\text{m}$  is an e-wave and the  $1.064 \mu\text{m}$  beam is an o-wave the indices are the same at  $22.7^\circ$ .

- 2.22. For nonlinear interactions in birefringent crystals, walkoff is an important factor. Plot the walk-off angle (in degrees) as a function of crystal orientation (from  $0$  to  $90^\circ$ ) for the crystal, BBO (see Appendix B for Sellmeier equations). Use a wavelength of  $0.6 \mu\text{m}$ . The orientation of the crystal is defined as the angle between the  $k$ -vector and the optic axis of the crystal. Where is walkoff zero?

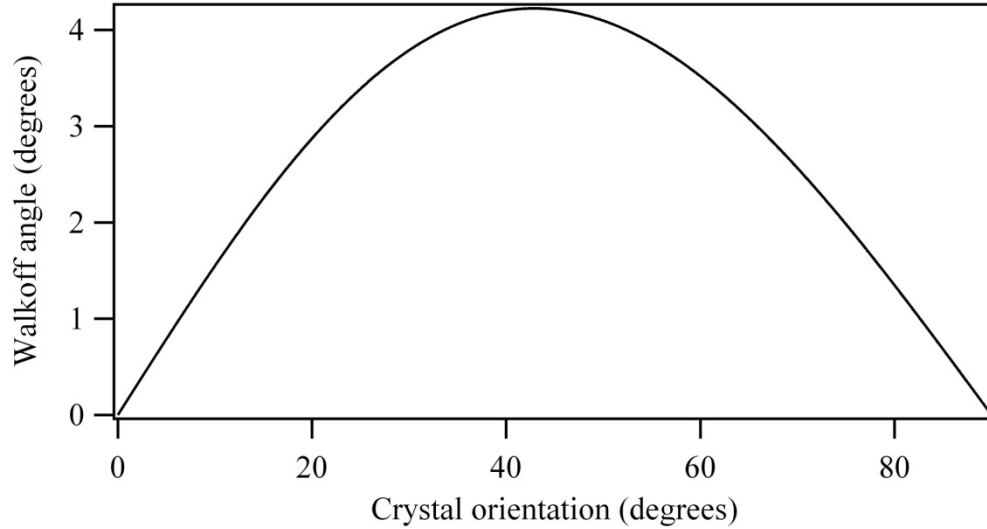


Figure S2.6. Plot of walkoff in BBO.  
Walk-off is zero at  $0$  and  $90^\circ$ .

- 2.23. Assume a beam waist is incident on a lens of focal length,  $f$ . The beam propagates a distance,  $d$ , where it is incident on a crystal that has an index  $n$ . Provided that  $d$  is less than the focal length, prove that the focused spot size in the crystal is the same as the focused spot size without a crystal. Also assume that the initial beam waist incident on the lens is large enough that the focused spot in air is a distance of approximately  $f$  away from the lens.

The ABCD matrix for the beam transformation going from the initial beam waist to the focused beam location is,

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & d_2 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ 0 & \frac{1}{n} \end{bmatrix} \begin{bmatrix} 1 & d \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix} = \begin{bmatrix} 1 - \frac{d}{f} - \frac{d_2}{nf} & d + \frac{d_2}{n} \\ -\frac{1}{nf} & \frac{1}{n} \end{bmatrix} \quad (\text{S2.68})$$

The starting  $q$  is a beam waist, so it is purely imaginary and we write it as  $iz_{R0}$ , where  $z_{R0} = \pi w_0^2 / \lambda$ . The  $q$  parameter after transformation is (see Equation 2.125),

$$\begin{aligned} q &= \frac{i \left( 1 - \frac{d}{f} - \frac{d_2}{nf} \right) z_{R0} + d + \frac{d_2}{n}}{-\frac{iz_{R0}}{nf} + \frac{1}{n}} = \frac{i(nf - nd - d_2)z_{R0} + dnf + d_2f}{f - iz_{R0}} \\ &= \frac{(dnf + d_2f)f - (nf - nd - d_2)z_{R0}^2}{f^2 + z_{R0}^2} + i \frac{(dnf + d_2f)z_{R0} + (nf - nd - d_2)z_{R0}f}{f^2 + z_{R0}^2} \end{aligned} \quad (\text{S2.69})$$

$$\begin{aligned} \frac{1}{q} &= \frac{f - iz_{R0}}{(dnf + d_2f) + i(nf - nd - d_2)z_{R0}} \\ &= \frac{f(dnf + d_2f) - (nf - nd - d_2)z_{R0}^2}{(dn + d_2)^2 f^2 + (nf - nd - d_2)^2 z_{R0}^2} - i \frac{nf^2 z_{R0}}{(dn + d_2)^2 f^2 + (nf - nd - d_2)^2 z_{R0}^2} \end{aligned} \quad (S2.70)$$

At the focus, the radius of curvature is infinite and hence the real part of  $1/q$  is zero. Therefore,

$$d_2 = \frac{(f - d)nz_{R0}^2 - ndf^2}{(f^2 + z_{R0}^2)} \quad (S2.71)$$

Substituting this expression back into Equation (S2.70) gives (we can ignore the real part since it is zero from the previous step)

$$\frac{1}{q} = -i \frac{f^2 + z_{R0}^2}{nf^2 z_{R0}}. \quad (S2.72)$$

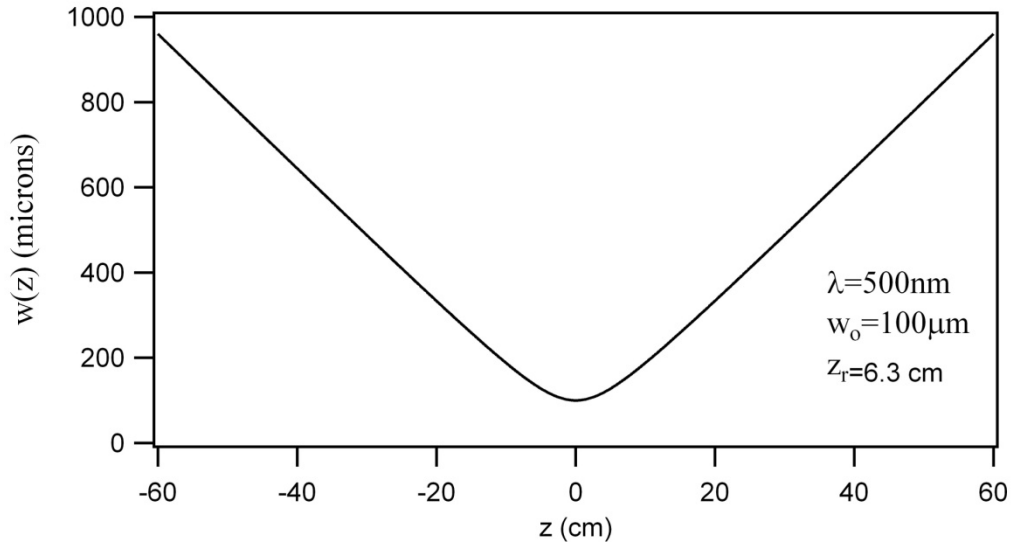
The beam size is found from Equation 2.122,

$$\frac{1}{q} = -i \frac{f^2 + z_{R0}^2}{nf^2 z_{R0}} = -i \frac{\lambda}{\pi n w_{\text{final}}^2} \quad (S2.73)$$

$$w_{\text{final}}^2 = \frac{\lambda}{\pi} \frac{f^2 z_{R0}}{f^2 + z_{R0}^2} \quad (S2.74)$$

Thus we see that the focused spot size has no dependence on the index of refraction.

2.24. Plot  $w(z)$  and  $1/R(z)$  for a Gaussian beam. Plotting the inverse of  $R(z)$  avoids problems near  $z=0$  where the radius of curvature is infinite. Assume that the wavelength is 500 nm, and that  $w_0=100\mu\text{m}$ . Plot from  $z=-10z_R$  to  $z=+10z_R$  where  $z_R$  is the Rayleigh range.



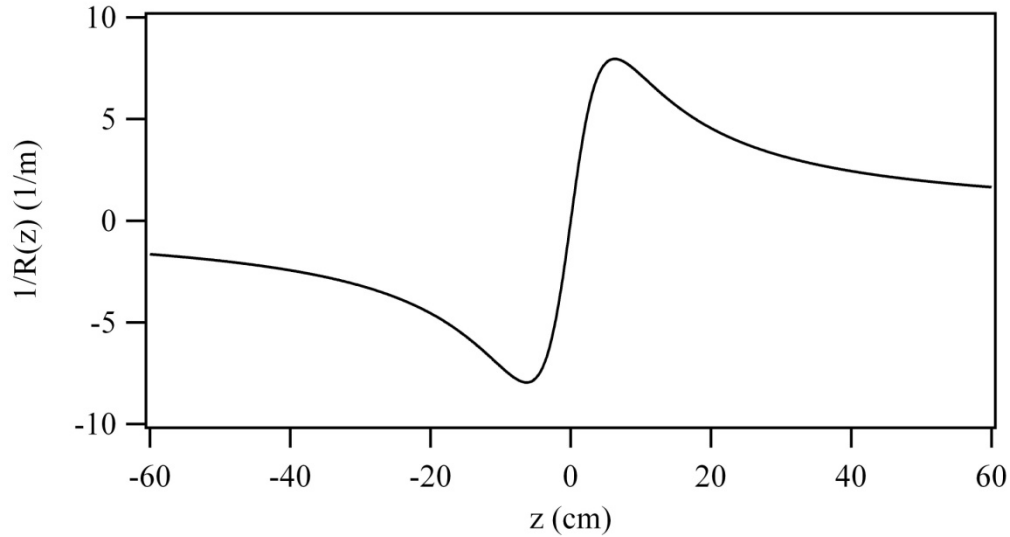


Figure S2.7. Top:  $w(z)$  and Bottom  $1/R(z)$  for Problem 2.24.

- 2.25. Three Gaussian laser beams are focused to have the same beam waist,  $w_0 = 200 \mu\text{m}$ , at  $z=0$  (radius of curvature  $=\infty$ ). The wavelength of the three lasers are  $\lambda_1 = 250 \text{ nm}$ ,  $\lambda_2 = 500 \text{ nm}$ ,  $\lambda_3 = 1000 \text{ nm}$ . Find the ratio of the Rayleigh ranges for laser1/laser2, and laser1/laser3, ie  $\frac{z_{R1}}{z_{R2}}$ ,  $\frac{z_{R1}}{z_{R3}}$ . Use the result to comment on beam overlap issues that arise for nonlinear interactions that require the overlap of beams with different wavelength.

The ratio of Rayleigh ranges for beams with the same  $w_0$  but different wavelengths is

$$\frac{z_{R1}}{z_{R2}} = \frac{\lambda_2}{\lambda_1}, \quad \frac{z_{R1}}{z_{R3}} = \frac{\lambda_3}{\lambda_1} \quad (\text{S2.75})$$

In the specific cases considered here,

$$\frac{z_{R1}}{z_{R2}} = \frac{\lambda_2}{\lambda_1} = 2, \quad \frac{z_{R1}}{z_{R3}} = \frac{\lambda_3}{\lambda_1} = 4 \quad (\text{S2.76})$$

Exact beam overlap is possible for only small distances since the different beams at different wavelengths diffract at different rates. Therefore this issue is important in nonlinear interactions where multiple beams at different wavelengths are interacting. The optimum spot sizes for the different beams is usually determined numerically.

- 2.26. Consider the optical system shown in Figure 2.14. A Gaussian beam waist ( $w_0$ ) is located a distance  $d_1$  from a lens of focal length,  $f$ . A distance  $d_2$  on the other side of the lens is a second beam waist.

- a) Use the Gaussian beam parameter,  $q$ , and the ABCD matrix approach to show that the distance,  $d_2$ , is given by the expression

$$d_2 = \frac{[(d_1 - f)d_1 + z_R^2]f}{(f - d_1)^2 + z_R^2}$$

where  $z_R$  is determined by the initial beam waist,  $w_0$  and is given by  $z_R = \frac{\pi w_0^2}{\lambda}$ . Hint, at a beam waist what is the radius of curvature and therefore what should the real part of  $1/q$  be?

- b) Show that the beam waist located at  $d_2$  is given by the relationship,

$$w_{\text{final}}^2 = \left[ \frac{f^2 z_R}{(f - d_1)^2 + z_R^2} \right] \frac{\lambda}{\pi}$$

- c) Consider a laser operating at  $1.064 \mu\text{m}$  that has a beam waist of  $200 \mu\text{m}$  at a location of  $1 \text{ cm}$  after the laser exit port. A certain nonlinear application requires us to focus this beam to  $w=130 \mu\text{m}$ . At what location(s) can we put a  $10 \text{ cm}$  focal length lens to obtain the desired spot size?

a) The ABCD matrix for the focusing system is,

$$\begin{bmatrix} A & B \\ C & D \end{bmatrix} = \begin{bmatrix} 1 & d_2 \\ 0 & 1 \end{bmatrix} \begin{bmatrix} 1 & 0 \\ -\frac{1}{f} & 1 \end{bmatrix} \begin{bmatrix} 1 & d_1 \\ 0 & 1 \end{bmatrix} = \begin{bmatrix} 1 - \frac{d_2}{f} & d_1 + d_2 - \frac{d_1 d_2}{f} \\ -\frac{1}{f} & 1 - \frac{d_1}{f} \end{bmatrix} \quad (\text{S2.77})$$

The Gaussian beam parameter is transformed according to

$$q_{\text{final}} = \frac{Aq_o + B}{Cq_o + D} = \frac{(f - d_2)q_o + (d_1 + d_2)f - d_1 d_2}{f - d_1 - q_o} \quad (\text{S2.78})$$

We note that because the beam starts at a beam-waist,  $q_o = iz_R$ . Taking  $1/q_{\text{final}}$  and setting the real part to zero gives (since the radius of curvature is infinite at the beam waist),

$$(f - d_1)[(d_1 + d_2)f - d_1 d_2] + (f - d_2)z_R^2 = 0 \quad (\text{S2.79})$$

We solve this for  $d_2$  as a function of  $d_1$ ,

$$d_2 = \frac{[(d_1 - f)d_1 + z_R^2]f}{(f - d_1)^2 + z_R^2} \quad (\text{S2.80})$$

Note that the geometric limit is obtained by setting  $z_R = 0$ .

b) The imaginary part of  $1/q_{\text{final}}$  is

$$\text{Im} \left[ \frac{1}{q_{\text{final}}} \right] = \frac{-(f - d_1)(f - d_2)z_R - ((d_1 + d_2)f - d_1 d_2)z_R}{((d_1 + d_2)f - d_1 d_2)^2 + (f - d_2)^2 z_R^2} = -\frac{\lambda}{\pi w_{\text{final}}^2} \quad (\text{S2.81})$$

The following relationships help with the algebra required for Equation (S2.81) and using  $d_2$  from Equation (S2.80):

$$f - d_2 = \frac{f^2(f - d_1)}{(f - d_1)^2 + z_R^2} \quad (\text{S2.82})$$

and

$$(d_1 + d_2)f - d_1 d_2 = \frac{f^2 z_R^2}{(f - d_1)^2 + z_R^2} \quad (\text{S2.83})$$

Substituting these equations into (S2.81) gives,

$$\text{Im} \left[ \frac{1}{q_{\text{final}}} \right] = -\frac{(f - d_1)^2 + z_R^2}{f^2 z_R} = -\frac{\lambda}{\pi w_{\text{final}}^2} \quad (\text{S2.84})$$

Solving for  $w_{\text{final}}$ ,

$$w_{\text{final}}^2 = \left[ \frac{f^2 z_R}{(f - d_1)^2 + z_R^2} \right] \frac{\lambda}{\pi} \quad (\text{S2.85})$$

c) Equation (S2.85) is rearranged to solve for  $d_1$  as a function of the given parameters,

$$d_1 = f \pm \sqrt{\frac{w_o^2}{w_{\text{final}}^2} f^2 - z_R^2}$$

For the parameters given,  $d_1 = 19.9 \text{ cm}$  or  $d_1 = 1.4 \text{ mm}$ . The  $19.9 \text{ cm}$  solution is usually more practical to implement since it gives more working distance between the lens and the  $130 \mu\text{m}$  beam waist.

2.27. Table 2.1 gives data for the beam radius ( $1/e$  field radius) of a laser beam as a function of position. The wavelength of the laser is  $1.064 \mu\text{m}$ .

Table 2.1 Beam radius as a function of position



$W(\mu\text{m})$	$z(\text{cm})$
54.4	0.125
44.5	0.135
39.5	0.145
32.5	0.155
26.2	0.165
21.9	0.175
16.3	0.185
12.0	0.195
10.6	0.205
11.3	0.215
14.1	0.225
19.1	0.235
24.0	0.245
31.1	0.255
37.5	0.265
41.7	0.275
48.1	0.285
53.0	0.295
58.0	0.305

a) Plot  $W$  vs.  $z$  and on the same plot include the curve

$$W(z) = W_0 \left[ 1 + M^4 \left( \frac{\lambda(z - z_0)}{\pi W_0^2} \right)^2 \right]^{1/2}$$

For this part of the problem set  $M=1$ . For the values of  $W_0$  and  $z_0$  estimate them based on the data.  $z_0$  is the location of the minimum beam waist and  $W_0$  is the minimum radius. Tweak the values of  $W_0$  and  $z_0$  to get a best fit for all the data. Include the best values of  $z_0$  and  $W_0$  on the plot.

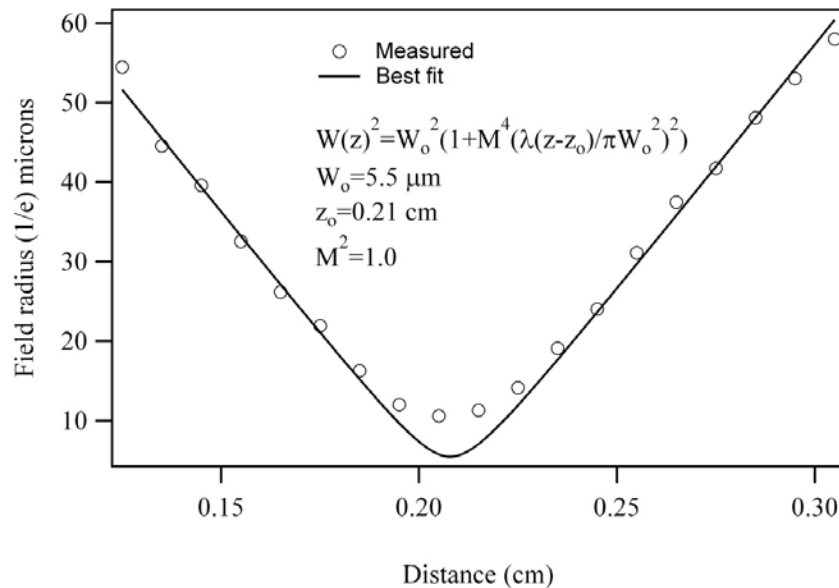


Figure S2.8. Plot for Problem 2.27 (a).

b) Using the results of part (a) as a starting point, perform a fit of the function  $W(z)$  above to the data to determine best values for  $W_0$ ,  $z_0$ , and  $M^2$ .

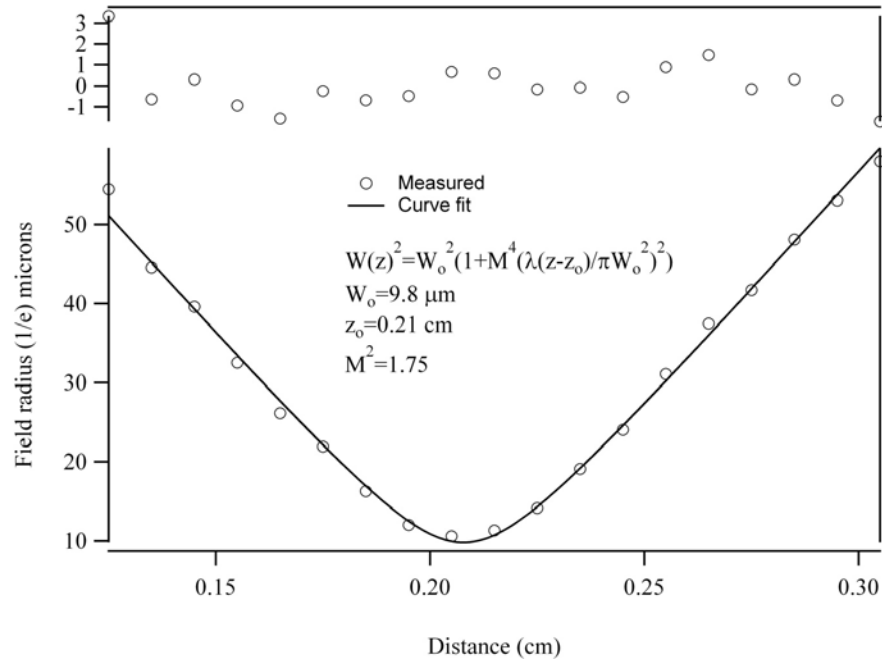


Figure S2.9. Plot for Problem 2.28 (b). The top part of the plot shows the residuals between the fit and the data.